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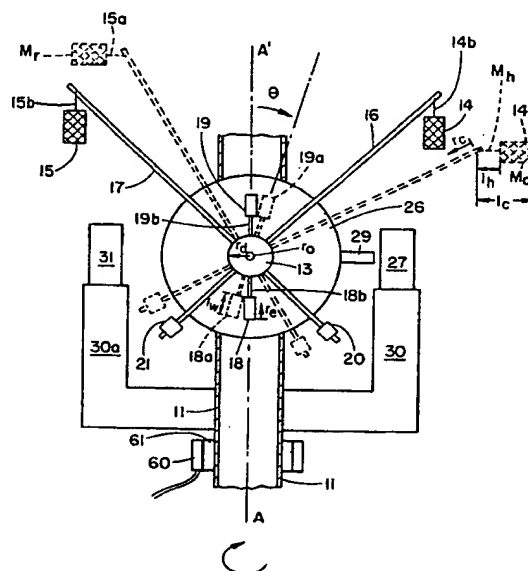
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⑤④ **Thermocentrifugometric analyzer.**

⑤⑦ A method and four devices for measuring the change in mass of a sample subjected to selected temperatures and fluid variables is disclosed. The test sample is subjected to centrifugal force to amplify the «apparent mass» of the sample by rotating the sample about a first axis of rotation. Any change in the mass of the test sample is then amplified by the centrifugal force and measured by the displacement of the sample about a second axis of rotation. The above method and four separate devices are disclosed. The first device balances the mass of the test sample against a known reference sample. The second device generates a counter-rotational force about the second axis to bring the sample to a «nulled» position. The third device balances the force generated about the second axis against a known and adjustable balance beam. A reciprocating means is used to couple the balance beam to a rotating sample holder. The fourth device generates a counter force along the balance beam to bring the sample to a «nulled» position. The devices are particularly adapted for mass change analysis in high temperature environments using high sweep gas rates and a variety of gaseous fluids.





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THERMOCENTRIFUGOMETRIC ANALYSIS

The present invention relates to a scientific instrument capable of performing conventional

5 thermogravimetric analysis. The instrument is also capable of measuring the mass of an unknown sample in ambient atmosphere. Further, the invention provides a heretofore unknown method of measuring the continuous mass change of a solid subjected to high sweep gas velocities. Further, the
10 invention will perform continuous mass change analysis with both high sweep gas velocities and elevated temperatures.

Conventional thermogravimetric analysis techniques are subject to fluctuating and unstable weight readings as the sweep gas flow past the solid being analyzed is
15 increased. The fluctuations not only reduce the accuracy of measurement at low gas flow rates, but may also grow very rapidly, totally invalidating thermogravimetric analysis weight readings even at moderate sweep gas flow rates.

J.M.Forgac and J.C.Angus, in "A Pressurized Thermobalance
20 Apparatus For Use at Extreme Conditions," (Industrial and Engineering Chemistry Fundamentals, Volume 18, No. 4, Page 416 (1979)) reported that the weight reading became unstable due to a natural convection current induced by the temperature difference between the gas and the solid.

25 This instability severely limits the application of thermogravimetric analysis techniques in the kinetic study of fast gas-solid reactions at elevated pressures and temperatures because:

(a) a high sweep gas rate, required to enhance the
30 contact between gas and solid and thereby determine the reaction kinetics (exclusive of external heat and mass transfer resistances) generates intense flow turbulences which cause instability of the weight measurement;

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1 (b) the flow turbulence generated increases as the
gas is compressed to elevated pressures. The compressed gas
then exerts an increased impact on the suspended solid;

(c) the temperature gradient developed about the
5 solid generates a free convection current which adds to the
flow turbulence.

The stability problems originate from the simple
fact that gravity is a very weak force field and is easily
disturbed by flow turbulences. It is generally considered
10 unavoidable in conventional thermogravimetric analysis
techniques. Due to the stability limitation of the
conventional gravimetric mass measurement, the sweep gas
velocity in conventional thermogravimetric reactors is very
restricted and is seldom allowed to exceed 0.1 m/s. In this
15 range of sweep gas velocity, the gas-solid mass and heat
transfer rates are very low, $Nu = 2$ as predicted by the
Froessling equation, and the reaction often proceeds in the
presence of significant temperature and composition
gradients. The limitation on the sweep gas velocity is most
20 pronounced at high pressures (high gas densities) and high
temperatures (thermal disturbances) typical of industrial
gas-solid reaction conditions.

The field of use for the present invention includes
not only its application as a scientific instrument in the
25 measurement of mass, but also in the duplication of
measurements obtained in conventional thermogravimetric
analysis. It also makes possible the measurement of the mass
change of a solid subjected to high sweep gas velocities at
elevated temperatures and pressures. Many industrially
30 important gas-solid reactions are conducted at elevated
pressures and temperatures such as those in coal
gasification, coal combustion, oil shale retorting, dolomite
sulfation, biomass pyrolysis, and mineral conversions.

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1 Thermogravimetric analysis has rarely been used for
liquid-solid contact systems because of the instability
problems. The strong centrifugal force field of the present
invention however makes possible the measurement of the mass
5 and its change of a solid immersed in liquid. The present
invention therefore also provides useful experimental means
for the kinetic study of liquid-solid reactions such as those
in coal liquification, leaching of minerals and ores, and
purification of polluted water by activated carbon.

10 A conventional thermogravimetric analysis is
disclosed in U.S. Patent 3,973,636 which issued to Hiroshi
Uchida on August 10, 1976. This device is essentially a
balance beam having a known reference material applied to one
15 end of the balance beam and a test sample applied to the
other end. The known reference material and the test sample
are then subjected to high temperatures while any change in
mass of the test sample is detected by an electromagnetic
pickup device.

20 A general summary of thermogravimetric techniques
may be found in "An Introduction to Thermogravimetry" by C.J.
Keattch, FRIC published by Heyden and Son, Ltd. in
cooperation with Sadtler Research Laboratories Inc., Page
1-14, 1969).

25 U.S. Patent 3,812,924 to Fletcher et al. on May 28,
1974 discloses a device for monitoring a change in mass in
varying environments. This device is a cantilever beam
device using a strain gauge as the transducer for reflecting
the change in mass of the sample.

30 The foregoing patents and the book excerpt describe
conventional systems for thermogravimetric mass analysis. As
discussed above, conventional systems are not capable of
measuring the continuous mass change of a test solid under
high sweep gas velocities.

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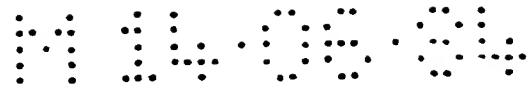
1 The two most widely used laboratory reactors for
fluid-solid reaction studies are described on pages 535 to
537 of the textbook entitled "Chemical Engineering Kinetics"
3rd Edition, authored by J.M.Smith, published by McGraw Hill
5 Book Company in 1981. These reactors provide uniform fluid
conditions and high fluid-solid contacting velocities.
However, they are not capable of measuring the changing mass
of the reacting solid. This textbook does describe on Page
640-642 a prior attempt to obtain uniform fluid conditions at
10 high fluid-solid contacting velocities in conventional
thermogravimetric analysis. This technique has had some
success with an extremely big and heavy single suspended
particle with a diameter greater than one inch. It is not
capable of handling ordinary solid particles which are much
15 smaller than one inch. The device illustrated, on page 641
(Figure 14-2) is a stirred-tank single-pellet reactor used
for the kinetic study of hydrofluorination of uranium
dioxide.

Basket-type mixed reactors are also used in
20 gas-solid contact systems. Such a device is disclosed in
pages 485-487 of "Chemical Reaction Engineering", 2nd Edition
by Octave Levenspiel, published by John Wiley and Sons, Inc.
in 1972.

The fluid-solid contact devices disclosed above are
25 not capable of measuring continuous mass changes in test
samples under high sweep gas rate velocities. Even in the
"stirred-tank single pellet reactor" the stirring speed is
very restricted due to the stability limitation.

The present invention uses centrifugal force to
30 amplify the weight of the sample to be tested. In
conventional thermogravimetric analysis, the weight of the
sample is determined by the gravitational pull on the mass of
the sample. In the present invention, the weight of the
sample is greatly amplified by centrifugal force.

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1 U.S. Patent 2,826,079 which issued to M.L.Kuder et
al. on March 11, 1958 discloses an automatic coin weighing
machine which in Figure 5 discloses a standard reference
weight indicated by the numeral 4, and a coin to be sampled
5 indicated by the numeral 5. If the coin is a counterfeit
coin the difference in weight between the standard reference
weight and the counterfeit coin will displace the center of
mass slightly from the geometric center of the wheel. The
apparatus then detects the displacement with an electronic
10 mutual inductance micrometer. This patent teaches the
concept of magnifying the apparent mass of the sample to be
tested by nearly 500 times. This magnifies the small weight
differential between the standard reference weight and the
counterfeit coin 500 fold.

15 U.S. Patent 2,814,944 to R.E. Brown issued on
December 3, 1957 discloses a centrifugal testing apparatus
for instruments. This device has some structural
similarities to the structures employed in one of the
embodiments of applicant's invention. In this device, a pair
20 of outwardly extending support arms rotate about a center
axis. Each of the outwardly extending support arms carries a
basket. One of the baskets is loaded with the instruments to
be tested, the other basket is loaded with the appropriate
counterweights to balance out the centrifuge. Dynamic
25 unbalance above a predetermined tolerance is detected
automatically and corrected by a servo-motor within the
mechanism. If the dynamic imbalance is too high, the
mechanism is shut down completely.

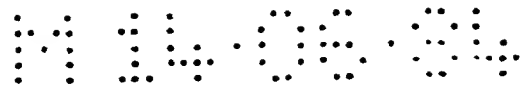
It should be noted that neither of the devices
30 illustrated in the Brown '944 patent nor the Kuter et al.
'079 patent are capable of measuring a mass change in a coin
or in the instrument. In addition, they are not capable of
measuring a mass change under extreme thermal conditions, or
under high sweep gas velocities and elevated temperatures and
35 pressures.

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The present invention discloses a process and several devices for measuring the change in mass of a test sample subjected to selected temperatures and fluid variables. The process includes the step of balancing the test sample against a known reactive force while the sample is suspended in an angularly displaceable sample receiving means. For each of the devices, the reactive force may be a known reference weight, or a null device which restores the angular rotation of the sample to a given null point. The sample receiving means is rotated about a first axis to amplify the apparent mass of the sample by centrifugal force. The speed of rotation may be held constant or may be varied. Changes in the speed of rotation may be used to dynamically balance the rotating mass, or to rebalance the rotating mass after a change in mass. When the desired apparent amplification of the mass has been achieved, the test sample may be subjected to selective temperature and fluid variables. The invention then measures the change in angular or radial displacement, or in the angular or radial displacement force generated by the test sample as it is subjected to the centrifugal force and the selected temperature and fluid variables. The change in mass of the test sample may then be measured by a derivative value of the change in displacement force, or a change in its angular or radial displacement.

In one embodiment of the invention, the thermocentrifugometric mass analyzer includes a rotating shaft and two rotor arms for balancing a test sample against a standard reference material. After compensating for gravimetric balance between the sample and the reference material, the two rotor arms are rotated at high speed while the test sample is subjected to thermal analysis, or fluid-solid interchange. As the two rotor arms rotate, any imbalance in the mass in the test sample over the mass in the standard



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1 reference will cause the rotor disc to be angularly
displaced. This displacement is a function of the difference
in mass between the known standard and the mass of the test
sample undergoing analysis. The angular displacement may be
5 measured and calibrated through a variety of techniques.

In a second embodiment of the thermocentri-
fugometric analyzer, the angular displacement of the rotor is
opposed by a null motor apparatus which senses the angular
displacement of the rotor and generates a counter-reactive
10 force to restore it to its original position. The amount of
reactive force necessary to maintain the rotor at the null
point is then used to measure the mass of the test sample.
In addition, the null point apparatus may be combined with a
variable speed motor to rebalance the device to achieve
15 dynamic balance, or to rebalance the device after a change in
mass. The mass measurement may then be derived from the
amount of reactive force, the speed of rotation or a
combination of both.

In a third embodiment of the present invention one
20 or more rotor arms are provided which are biased against a
balance beam positioned over a reciprocating rod connected
to the rotor arm. Means are provided for calibrating the
balance beam to provide a known reactive force for the sample
as it is subjected to centrifugal force. After the first
25 reference value is generated by the balance beam, any change
in mass in the test sample will be measured directly by a
change in the balance beam position as the test sample
undergoes analysis.

A fourth embodiment of the present invention
30 represents the null balance operation mode of the third
embodiment. The vertical displacement of the reciprocating
rod is opposed by a null balance device which senses the
vertical displacement and generates a counter-reactive force
to restore it to its original position. The amount of
35 reactive force to maintain the piston at the null point is
then used to measure the mass of the tested sample.

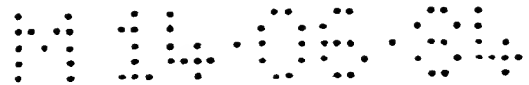
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1 Both the third and forth embodiments may be
combined with a variable speed motor to rebalance the device
to achieve dynamic balance, or to rebalance the device after
a change in mass. The mass measurement may then be derived
5 from the known reactive force, the null balance force, the
speed of rotation, or a combination of these forces.

In a fifth embodiment of the present invention,
several versions of the invention are used to establish a
radial displacement or a radial displacement force indicative
10 of the mass of the test sample or the change in mass of the
test sample. In addition, each of the radial displacement
devices may be combined with a variable speed motor to
provide an ability to dynamically balance the device, or to
compensate for a change in mass. In the latter instance, a
15 derivative value of the change in the speed of rotation can
be used to indicate the change in mass.

The present invention provides a thermocentri-
fugometric analysis as opposed to the previously known
thermogravimetric analysis. The thermocentrifugometric
20 analysis rotates the solid at high speeds, in which the
high-speed rotation not only provides very efficient
interchange between the gas and solid, but also generates a
very strong and stable centrifugal force field under which
the changing mass of the rotating solid can be continuously
25 measured. Since the centrifugal force field is several
orders of magnitude greater than gravitational force, the
measurement is extremely stable and not affected by gas-solid
flow disturbances.

Moreover, the present invention provides for the
30 amplification of the gravitational force field by centrifugal
force. A 5 cm long arm rotating at 2000 rpm will provide a
224 fold increase in the mass change of the sample to be
tested. By varying the speed of the rotation, there may be
varied the amount of centrifugal force applied to the test
35 sample. Thus the degree of amplification of the change in
mass may be varied to accommodate various fluid-solid
reactions.



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1 The proposed thermocentrifugometric analyzer has
potential use for a variety of gas-solid reaction studies,
both catalytic and noncatalytic, over a broad range of
applications from very fundamental surface reaction kinetic
5 studies to actual rate measurements under the simulated
conditions of industrial reactors. Some examples of its
potential applications are: combustion and gasification
studies on carbonaceous materials (carbon, coal, chars,
biomass); oxidation and reduction studies on metals and
10 ores; pyrolysis and calcination studies on decomposable
solids (coal, oil shales, biomass, limestones); silicon and
other solid deposition studies; and carbon deposition
studies on fouling catalysts.

 The remarkably stable mass measurement capability
15 of a thermocentrifugometric analyzer could also allow its use
for liquid-solid reaction studies for which the conventional
thermogravimetric analysis has seldom been used due to its
stability limitations. Some examples of its potential
applications are: adsorption studies on porous adsorbent
20 solids such as activated carbon, liquid leaching studies on
ores, and coal liquification studies.

 The present invention provides an extremely
accurate mass measurement device that will reflect a change
in mass at the nano-gram level of mass change.

25 It is therefore an object of the present invention
to provide a novel method of measuring the change in mass of
a test sample by rotating the sample about a first axis to
subject the sample to centrifugal force to amplify any change
in the "apparent mass" of the test sample.

30 It is another object of the present invention to
provide a method and several means for detecting the change
in the "apparent mass", by measuring rotational force
generated by test sample about a second axis of rotation.

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1 It is another object of the present invention to provide a method and several test instruments that will measure the change in mass at a high temperature and a variety of fluid conditions.

5 It is another object of the present invention to provide a centrifugometric mass analysis device that is capable of providing stable and continuous mass change readings when the test sample is subjected to elevated temperatures and pressures.

10 A further object of the present invention is to provide an instrument that will indicate continuous mass change readings when a material to be tested is subjected to elevated temperatures and pressures wherein the fluid is coacting with the solid at a high sweep fluid velocity. The
15 high speed rotation provides a relative velocity of 40 meters per second within a pressurized and heated autoclave when a 10 cm arm is used while rotating at 4000 rpm. Furthermore, the high speed rotation may be readily utilized for the
20 mixing of gas, which permits the operation of a thermocentrifugometric device as an integral mixed flow reactor.

 The present invention also provides a mass measurement device to determine the mass of any unknown sample by comparing it to a known reference material while
25 subjecting the test material and the reference material to a strong and adjustable centrifugal force.

 The present invention also provides a mass measurement device to determine the mass of any unknown sample by comparing it to a known and adjustable force while
30 subjecting the test material to a strong and stable centrifugal force.



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The foregoing objects and advantages of the centrifugometric mass analyzer may be more readily understood by one skilled in the art with reference being had to the following detailed description of the several preferred
5 embodiments thereof, taken in conjunction with the accompanying drawings wherein like elements are designated by identical reference numerals throughout the several views, in which:

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Figure 1 is a partially cross-sectioned and front view of the angularly displaceable embodiment of the present invention illustrated in a static state through solid lines, and in a dynamic state through dotted lines.

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Figure 2a is a diagrammatic illustration of a light emitter and flag used for measuring the angular displacement of the analyzer.

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Figure 2b is a diagrammatic illustration of a mutual inductance micrometer used to measure the angular displacement of the analyzer.

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Figure 2c is a diagrammatic illustration of an alternate embodiment using a mutual inductance micrometer mounted on the enclosure for measuring the angular displacement of the analyzer.

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Figure 3 is a partially cross-sectioned frontal view of a null motor embodiment of the present invention used in a sublimation study.

Figure 4 is an exploded isometric view of a portion of the null motor device illustrated in Figure 3.

Figure 5 is an isometric view of another portion of the null motor embodiment illustrated in Figure 3.

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1 Figure 6 is a cross-sectional view of a radiation reflector wherein the cross-section is taken along section line B-B' illustrated in Figure 5.

5 Figure 7 is a cross-sectional and diagrammatic view of another embodiment of the invention utilizing a reciprocal rod and balance beam.

 Figure 8 is a diagrammatic view of several alternate means that may be used to generate compensating forces to "null" the balance beam illustrated in Figure 7.

10 Figure 9 is diagrammatic illustration of an annular chamber that may surround the rotational path of a test sample to limit the circumferential flow of a fluid or gas induced by rotation of the sample.

15 Figure 10 is an isometric drawing illustrating a second embodiment for the sample retaining means that may be used with any embodiment of the present invention.

 Figure 11 is a schematic illustration of a null motor embodiment of the analyzer illustrated in Figure 14.

20 Figure 12 is a cross-sectioned and diagrammatic view of a quartz reactor that may be used with any radial displacement embodiment of the present invention.

 Figure 13 is an alternate embodiment of the present invention having a plurality of display means for indicating the angular displacement of the rotor in an autoclave.

25 Figure 14 is a partially cross-section frontal view of a null motor embodiment of the present invention illustrating its use in combination with an autoclave.

30 Figure 15 is a cross-section view illustrating the use of the embodiment illustrated in Figure 3 in an extremely high temperature autoclave.

35 Figure 16 is a cross-section and diagrammatic view of the analyzer illustrated in Figure 7 as adapted for use in an extremely high temperature autoclave when the device may be used as a thermocentrifugometric mass analyzer, or a conventional thermogravimetric mass analyzer.

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1 Figure 17 is a graph illustrating the accuracy of a
null motor thermocentrifugometric mass analyzed for the M_s
values and rotational speeds listed in Table 2.

5 Figure 18 is a diagrammatic illustration of a
motor control circuit used to control the speed of rotation
of the analyzer.

10 Figure 19 is a diagrammatic illustration of a
combined motor control and null balance control circuit used
to rebalance the analyzer through a change in the speed of
rotation.

15 Figure 20 is a partially cross-sectional and
diagrammatic view of a high-pressure, high-temperature
reactor utilizing a cantilever beam construction to measure
the radial displacement force generated by a rotating test
sample.

20 Figure 21 is a partially cross-sectional and
diagrammatic view of a high-temperature reactor with a
quartz reactor chamber that utilizes a load cell and a radial
displacement force arm to measure a change in mass.

25 Figure 22 is a partially cross-sectional and
diagrammatic view of a high temperature reactor with a quartz
reactor chamber with a radial displacement force analyzer,
using both a standard reference weight and a null force
generator.

30 The present invention relates to a process and
several forms of mechanical apparatus for carrying out the
process when it is desired to determine the change in mass of
a test sample when the test sample is subjected to selected
temperature and fluid variables. In conducting the process,
the test sample is balanced against a known reactive force
and suspended in an angularly displaceable receiver. The
known reactive force, as will be hereinafter described with
respect to the several mechanical embodiments of the
35 invention, may include a known reference weight, a null
motor, a balance beam, a radial displacement arm, a variable
speed motor, or one or more combinations of these.

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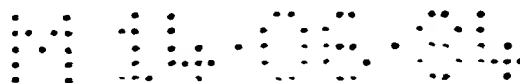
1 In measuring the change in mass, the sample and its
receiver are rotated about a first axis to amplify the
apparent mass of the sample by centrifugal force. Thus if
the initial mass of the sample were one gram, and the
5 reference weight were one gram, the apparent mass may be
amplified to 100 grams by selecting an appropriate speed of
rotation, and placing the sample receiving means at an
appropriate distance from the rotating axis. Both the speed
of rotation, and the radius of the circle traversed by the
10 sample may be varied to alter the apparent mass of the
sample. If the apparent mass were amplified by 1000 times, a
relatively small differential change in the mass of the test
sample may be easily determined by measuring the angular or
linear displacement of the sample. In an alternate
15 embodiment of the invention, this angular displacement about
a second axis is balanced by means of a null motor. In other
alternate embodiments of the invention, the angular
displacement is first converted to a vertical displacement of
a reciprocating piston placed along the first axis of
20 rotation. The vertical displacement is measured in a third
embodiment, and it is balanced by means of a measurable
counter-reactive force in a fourth embodiment.

While the device will measure mass by comparing an
unknown sample with a known reference material or force, it
25 is particularly suited for measuring the change in mass when
a test sample is subjected to one or more of the following
variables:

(a) a selected temperature or series of
temperatures substantially above or below the ambient
30 atmospheric temperature;

(b) a selected atmospheric pressure or series of
atmospheric pressures above or below ambient atmospheric
pressure;

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1 (c) a specific fluid-solid reaction wherein a
preselected test sample is rotated in a fluid or chamber
containing the reactant fluid;

(d) a selected high sweep fluid velocity or a
5 series of high sweep fluid velocities.

The sweep fluid velocities may be altered by a
plurality of means, such as the configuration of the sample
container, the speed at which the sample is rotated about its
first axis of rotation, the radius the circular path defined
10 by the sample, baffling and recirculation means to agitate
the gas within a test chamber, and external means for
directing a high sweep gas flow into the chamber to impinge
upon the rotating test sample.

The amplification of apparent mass as indicated
15 above is dependent upon the radius of the circle defined by
the test sample as it rotates, and the speed of rotation.
The following table sets forth the apparent amplification of
the mass at various radii of circular motion and rotational
speeds.

20	<u>RPM Of Test Sample</u>	<u>5 cm Arm Length</u>	<u>7.5 cm Arm Length</u>
	500	14 times M_s	21 times M_s
	1000	56 times M_s	84 times M_s
	2000	224 times M_s	336 times M_s
	4000	896 times M_s	1344 times M_s
25	5000	1400 times M_s	2100 times M_s

The arm length described above is the radius of the
circle defined by the test sample.

30 While the amplification of mass by centrifugal
force is a well-known principle of physics, it not heretofore
been applied to the field of thermogravimetric mass analysis.
As indicated previously, at extremely elevated temperatures
thermoconvection currents generated by the difference in
35 temperatures between the test sample and the reactive gas may

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1 render a conventional thermogravimetric mass analysis reading
inaccurate. The present invention provides a means of
amplifying the change in the gravimetric mass by a factor of
several hundred fold to assist in measuring the change as it
5 occurs through a change in temperature, a change in sweep
fluid velocity, a change in gas pressure, or a change in gas
composition.

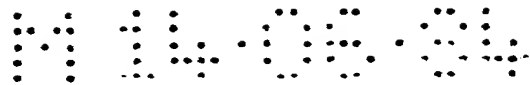
As indicated previously, the process of the present
invention may be practiced with several different mechanical
10 structures. These structures may be generally described by:

- (a) angular displacement apparatus;
- (b) null motor apparatus;
- (c) reciprocating shaft displacement apparatus;
- (d) reciprocating shaft null balance apparatus;
- 15 (e) radial displacement force apparatus;
- (f) radial displacement apparatus.

In addition, each of the foregoing devices may be used with a
variable speed motor for altering the apparent mass of the
sample.

20 The angular displacement apparatus may be
summarized as a centrifugometric mass analyzer for measuring
the continuous mass change of a test material subjected to
selected temperatures and other fluid variables. The
apparatus has a pair of angularly displaceable arms with a
25 sample receiving means located at the end of one arm, and a
known reference material receiving means located at the end
of the other arm. The arms are balanced for rotation about a
second axis of rotation. After initial balancing of the test
sample with one or more known reference weights, the device
30 is then spun or rotated about a first axis of rotation to
subject the test sample to centrifugal force. Any change in
the mass of the test sample then results in rotation of the
pair of arms about the second axis of rotation. This angular

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1 displacement is then measured. The change in mass of the
tested material may then be determined by a derivative value
of the change of angular rotation. A variety of methods and
means may be provided for measuring the angular displacement
5 of the rotating arms.

The null motor apparatus may be differentiated from
the angular displacement apparatus inasmuch as a null motor
is connected to the support means for the two rotating arms.
The null motor spins on the first axis of rotation with the
10 pair of rotating arms, and any change in angular displacement
about the second axis of rotation is immediately sensed by
the null motor apparatus and a counter force or reactive
force is generated to neutralize the angle of rotation and
restore it to a center "nulled" position. The mass of the
15 tested material and its change may then be determined by
measuring the counter rotational force applied by the null
motor to the angularly displaceable arms and its derivative
value.

The reciprocating piston displacement apparatus
20 may be distinguished from the above devices inasmuch as a
single angularly displaceable arm is provided for rotation
about a first axis. A known and adjustable reference force
is provided on the reciprocating piston placed along the
first rotational axis and the angular displacement of the
25 rotating arm and the tested solid exert a compressive or
extensive force on the piston. A measurement means is used
to measure the vertical displacement of the piston caused by
the difference between the reference force and the force
generated by the rotating arm and the tested solid. The
30 displacement is then used to determine the mass of the tested
solid by means of a calibration formula established prior to
the operation through a series of mass measurements on
various reference weights of known mass. A derivative value
of the displacement is used to determine the corresponding
35 derivative value of the change in mass as the tested solid is

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1 subjected to preselected temperature and fluid conditions.

The reciprocating piston null balance apparatus may be distinguished from the above reciprocating piston displacement apparatus inasmuch as a null device is connected
5 to the reciprocating piston. The vertical displacement of the reciprocating piston is immediately sensed by the null device and a reactive force is generated to neutralize the displacement and restore it to its original null position. The mass of the tested solid and its change may then be
10 determined by measuring the reactive force applied by the null device on the piston and its derivative value.

The radial displacement force apparatus may be distinguished from the foregoing device inasmuch as only a single axis of rotation is used. The outwardly depending arm
15 that connects the rotating shaft to the sample receiving means is normally perpendicular to the axis of rotation. As the sample receiving means is rotated, the radial force generated by the centrifugal force of the sample and sample receiving means is measured. As the sample undergoes a
20 change in mass, the radial force is altered, and the mass change may be calculated from the change in displacement force.

The radial displacement apparatus may be distinguished from the radial displacement force apparatus
25 inasmuch as the radial arm connected to the sample receiving means is allowed to reciprocate along a radial axis. In addition, reference weights and a null force generator may be added to offset the radial force generated by the rotating sample and sample receiving means.

30 In each of the foregoing embodiments the speed of the motor that drives the rotating shaft may be altered, thereby altering the apparent mass of the rotating sample. In this angular displacement apparatus, the speed may be decreased (as mass is gained) or increased (as mass is lost)
35 to maintain apparent mass at a constant value. Likewise,

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- 1 with the null devices, the speed may be increased or
decreased as the sample changes mass to balance a constant
null force. Alternately, either the rotational speed, or the
null force, or both may be altered to preselected values.
5 Altering the preselected rotational speed may also be
desirable to achieve a dynamic balance before mass change
experiments are begun.

As illustrated in Figure 1, the angular
10 displacement apparatus has a first axis of rotation indicated
by A-A' which is also the axis of rotation for shaft 11. A
means for rotating shaft 11 is illustrated in Figure 13 as
motor means 12. A support means 13 is rotatably mounted on
shaft 11 for rotation about a second axis indicated by r_o
15 in Figure 1. The second axis of rotation is perpendicular to
the first axis of rotation A-A'. A test material holding
means 14 is illustrated in Figure 1 in two states; a first
static state in which holding means 14 is illustrated in
solid lines, and a second dynamic state in which the holding
20 means 14a is illustrated in dotted lines. A reference
material holding means 15 is also illustrated in a first
static state by solid lines, and in the second dynamic state
15a by dotted lines. A first outwardly extending arm 16
connects the support means or rotor 13 with the test sample
25 holding means and a second outwardly extending arm 17
connects the reference material holding means to the support
means or rotor 13. Also mounted on the support means or
rotor 13 are a pair of compensator weights 18 and 19, which
are once again illustrated in a static state in solid lines,
30 and in a dynamic state in dotted lines as 18a and 19a.

Prior to the operation of the device, the apparatus
is balanced by means of adjusting the mass and location of
weights 20 and 21 to achieve both static and dynamic balance.
A test sample is then placed in the test material holding
35 means 14, and a reference material having a known mass

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1 characteristic is placed in the reference material holding means 15.

5 The apparatus is then rapidly rotated about axis A-A' as illustrated in Figure 1. Any difference in mass between the test sample and the reference material is reflected by an angular displacement about the second axis of rotation r_0 . As illustrated in Figure 1, the test material has gained mass relative to the reference material contained in the container 15. Any change in mass of the tested sample is reflected by a corresponding change in the angular displacement. If for example, the test were one in which the test material were subject to high temperatures to determine what gaseous components might be driven off, the change in mass in the test sample contained in the test material holding means 14 would be reflected by an angular displacement in the opposite direction as the test sample loses mass.

Means for measuring the angular displacement are illustrated in Figure 1 as a rotating indicator 26 and an angular displacement measurement means 27. Measurement means 27 may be mounted on the shaft 11 by means of vane 30, or may be fixably mounted within an enclosure such as the autoclave illustrated in Figures 13-16.

25 A variety of means for measuring the angle of rotation are illustrated in Figures 2a - 2d to match the instrument to the specific conditions that will be tested or measured. When the instrument is used under extremely high temperature conditions, most electronic transducers would prove to be either inoperable or ineffective because of nonlinear response characteristics. In these cases, optical means such as those illustrated in Figure 2a and Figure 2c are considered to be more effective in accurately measuring the angle of rotation. Figures 13, 14 and 16 also illustrate other ways of removing the means for measuring the angle of rotation from the autoclave chamber to an external location.

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1 In certain gas-solid and liquid-solid studies, the
turbulence of the fluid medium, or the reaction between the
gas and the tested solid may render an optical indication of
the angle of rotation extremely difficult to read. In such a
5 case, an electronic transducer such as illustrated in Figure
2b may be used in lieu of the optical means illustrated in
Figures 2a and 2c. The various means for indicating the
angle of rotation will be herewith discussed in detail with
respect to the discussions of the various embodiments of the
10 invention. As illustrated in Figure 14, a dummy rotor 25 and
the rotating indicator means 26 may have different sizes to
amplify or reduce the apparent angular rotation about r_0 .
By decreasing the size of the dummy rotor 25 one is able to
amplify the apparent angular rotation of rotor 26. This may
15 be desired to improve the accuracy of the angular reading.

Rotor 26 and dummy rotor 25 are connected by means
of a flexible drive member 28 which, in a practical
application, may be a chain or flexible wire. The material
is not important, but it is essential that all materials in
20 the construction of the device illustrated in Figure 1 be
capable of withstanding the temperature and atmospheric
conditions to which the test sample will be subjected. When
used in the autoclave enclosure illustrated in Figure 14, the
temperatures to which the sample may be subjected may range
25 from 200 to 2500°F.

The rotor units illustrated in Figure 1 require a
precision design because the instrument is intended to be
immersed in reacting fluid and generates the displacement
needed for measurement of the mass of the test sample. The
30 rotor disc is thin and light but needs to be relatively
strong and rigid and may be constructed of metal, ceramics or
quartz. Likewise, the outwardly extending arms 16 and 17 may
be formed of metal, ceramic or quartz. The test material
holding means 14 and the reference material holding means 15
35 may be small bowls, or baskets made of light and rigid

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1 material. Alternately, the material holding means may be
formed with a specific configuration as illustrated in Figure
10.

With respect to the angular displacement apparatus,
5 the arms 16 and 17 are positioned at 90° from one another to
ensure that the net moment of rotation generated by the two
rotor arms vanishes in all displacement angles of θ . This
positioning also provides the maximum possible angle of
displacement in either direction with respect to the net
10 change in mass of the sample being tested. Figure 1
schematically illustrates in dotted lines the rotational
displacement, and Table I (following) mathematically
describes the moment of rotation that causes the
displacement. The net moment of rotation generated by the
15 two rotor arms vanishes at all displacement angles θ when the
rotor arms are positioned at right angles to each other. A
net counterclockwise moment is generated by the baskets and
their hangers. This counterclockwise moment is compensated
for by a net clockwise moment generated by the compensator
20 weights 18 and 19. A very carefully calculated and designed
compensator can reduce the resulting residual moment to a
practical moment of zero over the entire range of the
operating displacement angle θ . As will be hereinafter
described, the desired design angle is -15° to $+15^\circ$. A fine
25 compensation for the net moment generated by the baskets and
hangers can be adjusted by adjusting the positions and mass
of compensator weights 18 and 19 along their support shafts
18b and 19b so that the residual moment of rotation can be
kept at less than: $2.5 \times 10^{-3} \times W^2 M_c r_c l_c [1 + (l_h/l_c)]$
30 acting in the direction of θ .

The residual moment vanishes at both $\theta = 0$ and $\theta =$
 $\pm 15^\circ$ and is maximum at $\theta = \pm 7.5^\circ$. Other ranges of θ could be
selected, but these could cause imbalance problems (when
extremely large) or give insufficient displacement for
35 reading (when extremely small). In addition, the relative



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1 angles of rotor arms 16 and 17 could be changed, but 90° has
been selected as the optimum operating angle for this
embodiment. For other embodiments, a different optimum
operating angle may be selected.

5 When the residual moment of rotation is well
compensated, the rotor assembly is dynamically well balanced
at all displacement angles, and the ratio of the solid mass
 M_s the material to be tested (placed in the right hand
side container illustrated in Figure 1) to the reference mass
10 M_r of the reference material (placed in the left hand side
container of Fig. 1) is related to θ by

$$\frac{M_s}{M_r} = \frac{[\cos(45 + \theta) + l_c/r_c] \sin(45 + \theta)}{[\cos(45 - \theta) + l_c/r_c] \sin(45 - \theta)}$$

15 As illustrated in Figure 1, Table I (following) and
the above formula:

- M_s is the mass of the sample to be tested
- M_r is the mass of the reference material
- M_h is the mass of the hanger (14b, 15b)
- 20 M_c is the mass of the container (14, 15)
- M_e is the mass of the compensator extension arm
(18b, 19b)
- M_w is the mass of the compensator weights (18,
19)
- 25 l_c is the length of the containers and hangers
from their point of attachment to the rotor arms 16 and 17
- l_h is the length of the hanger arm between the
rotor arm and the container
- l_w is the length of the compensator weights (18,
19)
- 30 r_c is the radius of the rotor arms at the point of
attachment for the hangers and containers 14, 14b, 15 and 15b
- r_e is the radius of the outer ends of the
compensator weights 18 and 19
- 35 r_d is the radius of the rotor disc 13
- W is the speed of rotation of the first axis
- T is the moment of rotation about the second axis

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1 TABLE I: MOMENTS OF ROTATION T/w^2

Rotor disc: net:zero

Rotor arms: net:zero

5 Container hanger

$$+ M_h r_c^2 [\cos (45 - \theta) + 0.5 (l_h/r_c)] \sin (45 - \theta)$$

$$- M_h r_c^2 [\cos (45 + \theta) + 0.5 (l_h/r_c)] \sin (45 + \theta)$$

$$\text{net: } -0.707 M_h r_c l_h \sin \theta$$

10

Container

$$+ M_c r_c^2 [\cos (45 - \theta) + 0.5 (l_h/r_c + l_c/r_c)] \sin (45 - \theta)$$

$$- M_c r_c^2 [\cos (45 + \theta) + 0.5 (l_h/r_c + l_c/r_c)] \sin (45 + \theta)$$

$$\text{net: } -0.707 M_c r_c l_c [1 + (l_h/l_c)] \sin \theta$$

15

Compensator extension arms (two)

$$\text{net: } + 2X (0.333) M_e r_e^2 [1 + (r_d/r_e) + (r_d/r_e)^2] \cos \theta \sin \theta$$

Compensator weights (two)

$$\text{net: } + 2X M_w r_e^2 [1 - (l_w/r_e) + 0.333 (l_w/r_e)^2] \cos \theta \sin \theta$$

20

Solid sample (RHS container)

$$\text{net: } + M_s r_c^2 [\cos (45 - \theta) + (l_c/r_c)] \sin (45 - \theta)$$

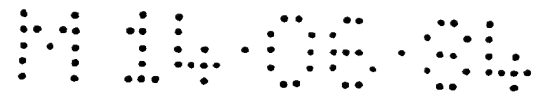
Reference mass (LHS container)

$$\text{net: } - M_r r_c^2 [\cos (45 + \theta) + (l_c/r_c)] \sin (45 + \theta)$$

25

30

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- 1 The design and mass of the compensator weights illustrated in Figure 1 is also based on the values selected for r_d , r_e , r_c , l_w , l_c , l_h , M_e , M_c and M_h .

- 5 In the design of the compensator weights illustrated in Figures 1, 2, 11 and 12, the residual moment of rotation is determined by:

$$10 \quad \frac{T_{\text{residual}}}{w^2} = \frac{T_{\text{net, container + hanger}}}{w^2} \left[\frac{1 + T_{\text{compensator + arm}}}{T_{\text{net, container, + hanger}}} \right]$$

Substituting the values of T listed in Table 1 gives:

$$15 \quad \frac{T_{\text{residual}}}{w^2} = -0.707 M_c r_c l_c [1 + (l_h/l_c) + (M_h/l_h/M_c l_c)] \sin \theta \cdot (1 - C \cos \theta)$$

in which compensator constant C is defined as:

$$20 \quad C = \frac{M_w r_e^2 [1 - (l_w/r_e) + 0.333 (l_w/r_e)^2] + 0.333 M_e r_e^2 [1 + (r_d/r_e) + (r_d/r_e)^2]}{0.354 M_c r_c l_c [1 + (l_h/l_c) + (M_h l_h/M_c l_c)]}$$

- The design of the compensator reduces to selecting a proper value of C so that $\sin \theta (1 - C \cos \theta)$ remains reasonably small over the entire range of the operating displacement angle, $-15^\circ < \theta < 15^\circ$. Two methods are tested in the following. In one, C is selected so that the residual moment vanishes not only at $\theta=0$ but also at $\theta = 15^\circ$. This is accomplished by choosing $C = 1/\cos 15^\circ = 1.0353$. In the other, C is selected so that the integral of $\sin^2 \theta (1 - \cos \theta)^2$ over $0 \leq \theta \leq 15^\circ$ is minimum. This least square fit gives $C = 1.0207$. The values of $\sin \theta$

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1 (1 - C cos θ) at various θ are given below for the compensator constants determined by these two methods.

5	θ (degree)	$\sin \theta \cdot (1 - C \cos \theta) \times 10^3$	
		<u>C = 1.0353</u>	<u>C = 1.0207</u>
	0	0	0
	2.5	-1.5	-0.9
	5.0	-2.7	-1.5
	7.5	-3.4	-1.6
10	10.0	-3.4	-0.9
	12.5	-2.3	0.8
	15.0	0	3.6

15 This indicates that the residual moment of rotation is relatively insensitive to the compensator constant over the range $1.021 < C < 1.035$, and either method is acceptable.

Once the compensator constant is selected, one can proceed to design the compensator using the above equation. In the test apparatus, with the following dimensions and mass constants, the above compensator constant equation provided
20 $M_w = 1.16$ g for $C = 1.0353$ and $M_w = 1.17$ g for $C = 1.0207$:

25

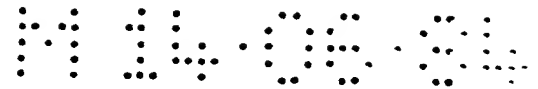
$$\begin{aligned} r_d &= 1.3 \text{ cm}; & r_e &= 2.3 \text{ cm}; & r_c &= 8.0 \text{ cm} \\ l_w &= 0.75 \text{ cm}; & l_c &= 3.0 \text{ cm}; & l_h &= 1.0 \text{ cm} \\ M_e &= 0.02 \text{ g}; & M_c &= 0.3625 \text{ g}; & M_h &= 0.0120 \text{ g} \end{aligned}$$

Thus, a compensator weight of mass 1.16 to 1.17g appears to be satisfactory for the test apparatus.

30 In this version of the test instrument, the linearity of the M_r/M_s vs θ relationship was extremely good over the range of $-0^\circ < \theta < 15^\circ$, and provided the following relationship:

35

$$\frac{M_r}{M_s} = 1 - 0.012\theta$$



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1 In this equation, it is understood that M_s M_r
 and therefore θ occurs in the direction of M_s . The same
 equation applies when M_s M_r , with the left hand side of
 the equation replaced by M_s/M_r . Over the entire range of
 5 operable θ , $0^\circ < \theta < 15^\circ$ in either direction, the measurable
 range of mass ratio is then given by $0.82 (M_s/M_r) 1.22$.

The range of mass ratio can then be translated into
 a window of mass measurement. When the reference mass is
 chosen to be the average of the initial and final masses of
 10 the tested solid, the apparatus is capable of measuring any
 mass change from a 33% decrease to a 49% increase relative to
 the initial mass. Larger mass changes can be accommodated by
 adding inert weights to both containers. For example, a mass
 change of 1 gram to zero can be measured by adding 2 grams of
 15 inert weights so that the total mass decreases from 3 grams
 to 2 grams, a 33% decrease. The range of mass ratio can be
 adjusted by varying the length of the container l_c relative
 to the position of container pin r_c . Although l_c/r_c
 greater than 0.4 is generally less desirable because of the
 20 resulting nonlinearity, any l_c/r_c less than 0.4
 increases both the linearity and the accuracy by narrowing
 the range of the mass ratio. Thus $l_c/r_c = 0.2$ gives $0.88 <$
 $(M_s/M_r) < 1.14$, or 23% decrease to 30% increase; and
 $l_c/r_c = 0.1$ gives $0.93 < (M_s/M_r) < 1.08$, or 14%
 25 decrease to 16% increase.

The accuracy in the measurement of the mass ratio
 against the displacement angle is effected by the residual
 moment of rotation, and its extent is determined by the ratio
 of the residual moment of rotation to the moment of rotation
 30

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1 generated by the reference mass. When the compensator is
designed as described above, a maximum of the ratio occurs at
 $\theta = \pm 7.5^\circ$ and is given by

$$5 \quad \left(\frac{\text{residual moment}}{\text{moment by reference mass}} \right)_{\max} = \frac{(2.5 \times 10^{-3}) M_c l_c (1 + l_h/l_c)}{M_r r_c (\cos 37.5 + l_c/r_c) \sin(37.5)}$$

10 In one embodiment of the invention, a test apparatus was
constructed in which

$$l_h = 1 \text{ cm}$$

$$l_c = 3 \text{ cm}$$

$$r_c = 8 \text{ cm}$$

the ratio then became:

$$15 \quad \left(\frac{\text{residual moment}}{\text{moment by reference mass}} \right)_{\max} = 2.0 \times 10^{-3} \cdot M_c/M_r$$

20 Therefore, insofar as the reference mass exceeded
one-fifth of the basket mass, the error caused by the
residual moment of rotation could be kept below one percent.
As is apparent from the above formula, different proportions
of l_h, l_c, r_c and M_c/M_r can also provide improved
accuracy.

25 As illustrated in Figure 1, in the angular
displacement apparatus, the two rotor arms are placed at
right angles to each other because the moment of rotation
generated by these arms must be exactly compensated for over
the entire range of the displacement angles. In the null
30 point apparatus illustrated with respect to Figure 2, this
angle is determined by the total moment of rotation generated
by the rotor arms, the mass containers and other parts
mounted on the rotor, and need not be 90° . It has been found
however that extremely small angles or extremely large angles
35 cause a disturbance in the relative angular displacements of
arms 16 and 17. This disturbance can then affect the
accuracy of the readings.

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1 As illustrated in Figure 1, the rotating shaft 11
has attached thereto a pair of vanes 30, 30a, which may be
used to agitate the gaseous medium within a autoclave or
other enclosure. A transducer means 27 is mounted on vane 30
5 to respond to flag means 29 which is fixably mounted to
indicator disc 26. Transducer means 27 responds to the
position of flag 29 to provide an electrical indication of
the angular displacement of disc 26 and arms 16, 17. A
compensator weight 31 is added to vane 30a to balance the
10 rotational moment generated by the angular displacement
measuring device 27. A pair of slip rings 60 and 61 are
provided to translate the electrical signals generated by
transducer 27 from a rotary environment to a stationary
environment. Slip ring 61 is mounted on shaft 11 and rotates
15 with the shaft, while slip ring 60 is stationary, and mounted
on a stationary portion of the enclosure. The operation of
the transducer means 27 and flag 29 will be hereinafter
explained with respect to Figures 2a - 2d.

Figure 2a illustrates a physical light obstruction
20 flag 29a and is mounted on rotor 26. The light obstruction
flag 29a traverses slot 67 in the transducer 27a as the rotor
disc 26 is rotated. A light emitter 65 is used to provide a
beam of light that transverses slot 67 and energizes
photo-sensor 66. When in the central or nulled position, the
25 light flag 29a totally obscures the light path between the
light emitter 65, and the photo-sensor 66. As rotor disc 26
is rotated, however, a gradually larger signal is generated
by photo-sensor 66.

30 Illustrated throughout Figures 2a - 2d are gravity
compensation weights 64a - 64c, and centrifugometric
compensation weights 63a - 63d.

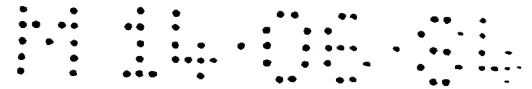
In the embodiment illustrated in Figure 2b, a metal
chip is mounted on the flag 29b. The transducer 27b then
takes the form of a mutual inductance micrometer mounted for
35 rotation on vane 30. While it is depicted in a vertical

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1 position in Figure 2b, it should be understood that the
positioning of the mutual inductance micrometer 27b could
also be as illustrated in Figure 1, adjacent the flag 29b.
The output of the mutual inductance micrometer 27b is then
5 conveyed to the slip ring 61 for output to the stationary
slip ring 60 to a display and control means as will be
hereinafter later described.

As illustrated in Figure 2c, a mirror 68 is mounted
on the flag 29c. The transducer 27c takes the form of one or
10 more parallel light sources 69 and a series of
microphoto-sensors arrayed as illustrated at 27c in Figure
2c. As disc 26 rotates, the mirror 68 reflects the light
back as indicated by arrow 70 to energize one or more of the
series of microphoto-sensors. As the rotor 26 is rotated,
15 the relative path light beam 70 traverses the length of the
series of microphoto-sensors 27c to provide an indication of
the angle of rotation.

As illustrated in Figure 2d, the flag 29 has been
replaced with a circular disc ring, 29d, that serves a
20 similar function to the metal chip mounted on flag 29b
illustrated in Figure 2b. The transducer 27d is again a
mutual inductance micrometer that may be fixably mounted in
the enclosure. Inasmuch as the flag 29d is a continuous
circular ring, it will provide a steady output signal for the
25 mutual inductance micrometer that is a function of the
angular rotation of disc 26. As illustrated in Figure 2b,
the transducer 27b, is mounted on the rotating portion of the
apparatus will provide a steady output that is function of
the distance between the metal chip and the inductance
30 micrometer. If the transducer 27b illustrated in Figure 2b
is mounted on the enclosure, then the metal chip 27b would
generate a series of pulses, the amplitude of which would
vary as the disc 26 is rotated. By utilizing the angular
ring illustrated in Figure 2d, a steady output signal is
35 derived which is a function of the angular rotation of
disc 26.



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Figure 3 illustrates a second embodiment of the thermocentrifugometric analyzer wherein the angular displacement of the rotor 13a is opposed by a null motor apparatus which senses the angular displacement of the rotor and generates a counter reactive force to restore to its original position. The amount of reactive force necessary to maintain the rotor at the null point is then used to measure the mass of the sample. While the device illustrated in Figure 3 is illustrated in a static position, it is understood that it rotates rapidly on shaft 11 about axis A-A' as was previously explained with respect to Figure 1. Rotor arms 16 and 17 normally suspend a sample holder 14 and a reference weight holder 15 as was illustrated with respect to Figure 1. In Figure 3, however, the sample holder has been replaced with hanger 16e and a sublimating or "evaporating" sphere of naphthalene. Naphthalene is used as a typical example of a solid for which gaseous reaction studies might be desired. The reference weight holder 15 has been replaced with hanger 17e and a reference weight lead shot 15e. Alternately, the reference weight 15e may be replaced by a fixed and linearly displaceable weight 15c illustrated in dotted lines in the lower most portion of arm 17 in Figure 3. The mass of weight 15c is used to compensate for the mass of the sample material illustrated at 14e.

A coil 202 is formed about rotor 13a as will be hereinafter explained with greater detail with respect to Figure 4. A current is supplied to coil 202 through slip ring commutators (not shown) as the shaft 11 is rotated. A fixed magnet 201 is mounted on one side of rotor coil 202, and a variable electromagnetic coil 203 is placed on the other side of rotor coil 202. The current for coil 203 is also supplied through a slip ring commutator in a manner similar to that supplied to coil member 202. In addition, if the loading of the device warrants, the magnetic field crossing the coil may be enforced by placing a highly permeable ferromagnetic material inside, but not in contact

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1 with the rotor 13a. In addition, a polarized electromagnet
may be used to strengthen the magnetic field surrounding the
coil 202.

Application of a current to coil 202 will result in
5 magnetic lines of force aligned along axis A-A'. The use of
magnets 201 and magnets 203 will tend to maintain the coil
202, and thereby rotor 13a in the position illustrated in
Figure 3. As a change in mass is experienced by sample 14e,
the imbalance will generate a rotational moment about r_o at
10 the center of rotor 13a. If there is a change in mass
wherein the sample 14e loses mass, rotor arm 16 will be
displaced downwardly as illustrated in Figure 3. If the
reaction generates additional mass in the sample 14e, rotor
arm 16 will be displaced upwardly. The relative rotational
15 moment of rotor arms 16 and 17 about r_o is opposed by the
electromagnetic force generated on coil 202 subjected to the
magnetic field generated by magnet 201 and coil 203. The
relative rotational displacement of rotor 16a is measured by
flag 29e, and transducer 27e in a manner similar to that
20 previously described and illustrated with respect to Figures
2a - 2d. Either a light detector, or a mutual inductance
micrometer may be used. Any change in the position flag 29e
will immediately be detected by transducer 27e, and
communicated via slip ring commutators 204 and 205 to the
25 electronic control circuitry for the thermocentrifugometric
mass analyzer. Appropriate corrective currents will then be
supplied through the stationary slip ring commutator 204, and
the rotary commutator 205 to coil means 203 to apply a
corrective force to armature coil 202 that surrounds rotor
30 13a. By measuring the change in current supply to coil 203
that is required to rebalance rotor 13a to its central nulled
position, one is able to determine a functional value that is
representative of the change of mass in the sample 14e.

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1 The details of the device illustrated in Figure 3
are further illustrated in Figures 4 - 6. The rotor 13a
comprises an elongate cylinder having a coil 202 wrapped
around its center axis. Rotor 13a is supported for rotation
5 by means of pins 208 and 209 in jeweled bearings 210 and 211.
The jeweled bearings 210 and 211 are secured by jewel ring
holders 212 and 213 which are threadably secured in apertures
214 and 215 (not shown) in shaft 11a as illustrated in Figure
5. The use of pins 208, 209, and jeweled bearings 210 and
10 211, together with the threadable jewel ring holders 212 and
213 provide for very precise positioning of the rotor 13
within the enlarged shaft member 11a. The compensator
weights 206 and 207 are secured to rotor 27a by means of rods
216 and 217. While end brackets 206 and 207 form part of the
15 compensator weight, additional compensator weights may be
provided as illustrated at 218 - 221 to compensate for the
coil balance displacement flag or other structural features
of the rotating parts of rotor 13a. The flag means 29e
reciprocates within slot 67e as rotor 13a pivots about pins
20 208 and 209. In doing so, it varies the output of
photo-sensor 66e. A light emitting diode, or other light
emitter 65e is focused on photo-sensor 66e, and is partially
occluded when in the central balanced or nulled position by
means of flag 29e.

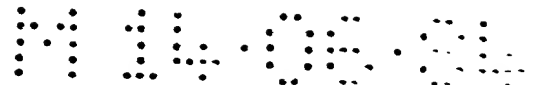
25 As illustrated in Figure 5, shaft 11 contains an
enlarged portion 11a for containing the rotor 13a. Formed
within the enlarged shaft portion 11a is a transducer
mounting plate 222 having a slot 223 formed therein for
receiving the flag 29e. In addition, when used in an
30 extremely high temperature environment, the rotor is equipped
with high temperature shielding or radiation reflecting means
224 which is more fully illustrated in Figure 6. The conical
portion 11b of shaft 11 is protected by means of insulation
224a and a radiation reflector 224b to prevent the intense
35 heat generated by the high temperature autoclave from

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1 reaching the electrical components mounted within the
enlarged shaft 11a. The need for the radiation reflector and
insulation will be more fully illustrated with respect to the
device illustrated in Figure 15.

5 An alternate embodiment for the null point
apparatus for measuring the change in mass in accordance with
the principles of the present invention is illustrated in
Figure 14. As illustrated in Figure 14, a rotary disc 13,
the support arms 16 and 17 and the baskets 14 and 15 are
10 essentially the same as those described previously with
respect to Figure 1. Although it is illustrated in a static
position in Figure 2, in operation it is rapidly rotated
about axis A-A' by means of shaft 11 and motor means 12. The
relative angular displacement of rotor 13 is transferred by
15 the flexible linkage 28 to dummy rotor 25 which is now
mounted below the autoclave chamber 40. The flexible drive
means 28 is guided by means of rollers 36, 37, 38 and 39
within shaft 11 to provide a relatively friction free
transfer of the relative angle of rotation from rotor disc 13
20 to dummy disc 25. Tensioning means 32 and 33 maintain
appropriate tension level on flexible drive means 28. In the
preferred embodiment, a thin wire chain was used to transfer
the angular rotation from rotor 13 to dummy disc 25. As
indicated previously with respect to Figure 1, the angular
25 displacement can be read directly by optical means, or can be
converted into an electrical signal by hydraulic, electrical,
magnetic, or optical means. In the null point apparatus
illustrated in Figure 3, however, the angular displacement
generates an electrical signal in a displacement measuring
30 means 43 (illustrated in Figure 11). Control means 42 is
responsive to the signal and responds by energizing motor
means 41 to generate a reactive force along drive means 45 to
the dummy rotor 25. The reactive force is then transmitted
by a flexible drive means 28 to the rotor 13. In the null
35 point apparatus, motor 41 is a two poled DC motor placed on a



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1 supporting frame 46 which is fixed on rotating shaft 11. A
compensator weight 47 is provided to maintain an effective
balance for the null point apparatus during the high speed
rotation of shaft 11. A pickup brush 48 is used to transfer
5 the input and output signals and power for motor means 41
from the stationary support 49b to the rotating shaft 11.
The electrical signals picked up by brush 48 are transmitted
by a control line 50b to the control unit 42.

A schematic of the null point apparatus is
10 illustrated in Figure 11 wherein 13 refers to the rotor, 25
the dummy rotor, 41 the motor means, and 43 the displacement
measuring means for measuring the angular displacement of
dummy disc 25. The signal generated by measuring means 43 is
transmitted by control line 50b to control device 42 which
15 energizes the motor 41 through control line 50a to restore
the angular rotation of dummy disc 25 to its central "nulled"
position. The restoring force is then transmitted along the
flexible means 28 to rotor 13 when the speed of rotation is
varied, the null force is related to the speed of rotation.
20 This relationship will be further explained hereinafter in
the Detailed Description of the Speed Regulation Mode.

As illustrated in Figure 14, the invention is
particularly adapted for use in a heated autoclave unit for
high temperature reaction studies. The instrumentation
25 chamber 49a can be protected from being overheated by
providing a cooling jacket 55 having a source of cooling
water at 56 and an outlet for the coolant at 57. This not
only provides for cooling of shaft 11, but also insulates the
autoclave unit 40 from the instrumentation chamber 49a. The
30 autoclave unit 40 utilizes conventional means for heating the
interior of the chamber to extremely high temperatures.
These studies may be conducted at any temperature from 200 to
2500°F. An instrumentation probe 57 is connected to a
control means 58 for maintaining the autoclave at the desired
35 thermal temperature(s). In addition to the thermocentrifugo-
metric analyzer, the rotating shaft 11 also has a pair of
agitator blades 59 and 60 to enhance gas mixing within the
autoclave. In addition, electrical heating elements may be

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1 placed in the agitator blades 59 and 60 to assist in
maintaining the interior of the autoclave at a constant
temperature. A gas inlet conduit 61 and a gas outlet conduit
62 are provided for admitting and discharging reactive gases
5 when it is desired to conduct a mass analysis with a specific
gas in lieu of ambient atmospheric air. If desired, the gas
inlet may be placed directly in line with the dynamic
position of containers 14 and 15 to direct high speed
impingement of the gas supplied through conduit 61 into the
10 path of container 14. In addition, chamber 40 may be
pressurized by means of conduit 61 and 62 to provide mass
analysis under high pressure gas conditions.

The control device 42 is equipped with a suitable
display 50 for indicating the amount of the reactive force
15 generated by motor means 41 and applied to the rotor disc 13.
Alternately, it may display a derivative signal which is
indicative of the change in mass indicated by the amount of
reactive force needed to maintain dummy disc 25 and rotor 13
and their central "nulled" position.

20 In the third embodiment of the present invention,
one or more rotor arms are provided which are pivotally
biased against a balance beam by means of a reciprocating
piston connected between the beam and the rotor arm. Means
25 are provided for calibrating the balance beam to provide a
known reactive force for the sample as it is subjected to
centrifugal force. After a first reference force is
generated by the balance beam, to affect the apparent mass of
the sample, any change in mass in a test sample will be
30 measured directly by a change in the balance beam position.

The reciprocating piston displacement apparatus may
be distinguished from the above devices inasmuch as a single
angularly displaceable arm 319 is provided for rotation about
a first axis A-A' as was previously described with respect to
35 Figures 1 and 3. A known and adjustable reference force is



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1 provided on the reciprocating shaft 320 that is aligned along
the first rotational axis A-A', and the angular displacement
of the rotating arm and tested solid exert a compressive or
extensive force on the piston. A balance beam measurement
5 means 321 is used to measure the vertical displacement of the
piston caused by the difference between the reference force
and the force generated by the rotating arm and the tested
solid. The displacement is then used to determine the mass
of the tested solid by means of a calibration formula
10 established prior to the operation through a series of mass
measurements on various reference weights of known mass. A
derivative value of the displacement is used to determine the
corresponding derivative value of the change in mass as the
tested solid is subjected to preselected temperature and
15 fluid conditions.

As indicated in Figure 7, the displaceable arm 319,
may be angled upwardly as illustrated by the solid lines, or
angled downwardly by the dotted lines 319a. The material to
be tested is placed in basket 314 which is suspended from arm
20 319 by means of hanger 314b. The rotational movement of
shaft 311 is imparted to the reference container by means a
motor as illustrated in Figures 13 and 14. Support arms 362
and 363 may also serve as circulatory vanes to agitate the
fluid or gaseous mediums surrounding the sample container
25 314. The compensator weight 365 is provided on arm 363 to
compensate for the relative mass of arm 319 and 319a, and the
weight of basket 314. As the device illustrated in Figure 7
is rotated about axis A-A', a rotational moment is generated
about axis 364 urging the rotor arm 319 outwardly and
30 displacing the reciprocating shaft 320 upwardly as
illustrated in Figure 7. Reciprocating shaft 320 is provided
with bearing means 322 and 323 which are used on either end
of reciprocating rod 320 to minimize the frictional drag that
may be generated between the rotation of rotor arm 319a
35 caused by the rotation of shaft 311, and the stationary

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1 position of balance beam 321. To further assist in
translating the rotary forces to a stationary balance beam,
an adjustable platter 324 is provided between the
reciprocating shaft 320, and the balance beam 321. A jeweled
5 bearing 325 is used between the platter and the balance beam
to translate the vertical movement of reciprocating rod 320,
to the angular movement of balance beam 321, about axis 326.
The relative movement of balance beam 321 may be detected by
transducer 327 or 327a (illustrated in dotted lines) in a
10 manner previously
illustrated with respect to Figures 2a - 2d. As illustrated
at 327, a photo-optical transducer is used with a flag 329
attached to the end of balance beam 321. Alternately, a
metal chip or magnet 329a may be attached to the balance beam
15 to activate a micro inductive coupler 327a.

A plurality of spring loaded adjusting screws
illustrated at 340 and 341 in Figure 7 are used to precisely
align platter 324 in a horizontal position with respect to
stationary support means 342.

20 In operation of the device illustrated in Figure 7,
the mass M_s of the test sample is compensated for by means
of an adjustable spring means 343 which exerts a compressive
or upward force on balance beam 321a. An adjustable weight
344 is moved along balance beam 321 to a predetermined
25 position that is determined by the weight of the sample to be
placed in test sample basket 314. A predetermined position
of weight 344 is calculated for a variety of rotational
speeds for shaft 311 and a variety of weights in said M_s
that may be placed in basket 314. Thus, in the operation of
30 the device, when the shaft 311 has reached its predetermined
rotational speed, with mass M_s in basket 314, the balance
beam will be balanced. The force generated by spring balance
343, and the position of displaceable balance weight 344 is
balanced against the apparent mass of the rotation sample at
35 a predetermined speed. As the sample M_s gains or loses

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1 mass in its reaction with the fluid or gaseous medium
surrounding basket 314, the rotational force is first
generated about axis 364, which is translated into vertical
reciprocation of reciprocating shaft 320. The vertical
5 movement is then translated through platter 324 to balance
beam 321, and measured by transducers 327 or 327a.

The embodiment illustrated in Figure 8 generates
reciprocal forces along reciprocating shaft 320b in a manner
identical to that previously described with respect to Figure
10 7. The forces generated along balance beam 321b, however,
are different from those generated along balance beam 321 and
321a illustrated in Figure 7. A variety of means illustrated
as 350, 351 and 352 may be used to provide a compensating or
restoring force to the balance beam to maintain it in a
15 central or nulled position. The amount of force necessary to
restore the balance beam to its nulled position may also be
derived by means of more than one technique.

As was previously illustrated with respect to
Figure 7, the upwardly generated force at point 325b on
20 balance beam 321b is opposed by spring means 343b, insofar as
the force is generated by the mass of arm 319 and hanger 314.
The force generated by M_g at the rotational speed and
weight selected and placed in hanger basket 314 is
compensated for by adjustable weight 344b. Means 350, 351
25 and 352 all provide means of generating additional
compensatory forces to restore the balance beam to a central
nulled position. In a first version of the null device, the
transducer 327b detects movement of a metal or magnetic chip
329b on the balance beam 321b. As movement of the balance
30 beam is detected, a compensating force is applied by any one
of the means 350, 351, or 352. The device illustrated at
350, is an adjustable point gravimetric balance which will
apply a counter force to spring 343b, depending upon the
electrical force transmitted to it by appropriate control
35 circuitry (illustrated in Figures 11 and 14). Alternately, a

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1 motor 351 may be used to exert a rotational torque about axis
326b on balance beam 321b. In a third embodiment of the null
point balance beam apparatus, a compressive type null device
352 may be used in lieu of the adjustable weight 344b to
5 provide an adjustable downwardly displaceable weight on
balance beam 321b. As the balance beam 321b is deflected
upwardly or downwardly by a change of mass M_s in container
314, the amount of force generated by the compressive type
null device 352 changes to restore the balance beam 321b to a
10 center nulled position.

Alternately, the device 351 illustrated as a motor
in Figure 8, may be replaced by a displacement measuring
means to measure the angular displacement of balance beam
321b. The control device (not shown) will then cause a
15 compensating force to be generated by means 350 or 352.

While an electrical means has been disclosed in
Figures 11 and 14, it should be understood that the
compensating forces generated by means 350, 351 and 352 could
be created electrically, hydraulically, magnetically, or
20 pneumatically, as desired. Each of the respective modes of
operation has distinct advantages, depending upon the
operating parameters and conditions in which the device will
be operated.

The test results from a thermocentrifugometric mass
25 analyzer using a null motor to generate a counter restoring
force is illustrated in Figure 17, using the M_s values and
rotational speed listed in Table 2.

TABLE 2

30	Test solid mass* M_s (milligrams)	Null current required (milliamperes)		
		600 rpm	1200 rpm	1500 rpm
	1.9 ± 0.1	12.5	50.0	79.0
	4.2 ± 0.1	29.0	115	180
	5.4 ± 0.1	37.5	150	235
	6.4 ± 0.1	43.5	175	275
35	0.2 ± 0.1	62.5	250	390

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1 *measured by a conventional gravimetric balance with an accuracy of 0.1 milligrams.

As illustrated in Figure 17, using the null motor balance, the null current required, i , is proportional to the
5 test solid mass, M_s and the square of the rotational speed, f , or

$$i = \frac{1}{K} M_s f^2 \quad \text{or} \quad M_s = K \frac{i}{f^2}$$

10 in which the proportionality constant, K can be calculated from the geometry of the coil and the magnetic field strength. However, when the magnetic field strength is difficult to measure, a plausible alternative to the calculation procedure is to determine it from a linear regression of preselected test data. Thus for this
15 particular balance

$$K = 5.26 \times 10^4$$

when i is in milliamperes, M_s is in milligrams and f is in rpm. As illustrated in Figure 17 the gravimetrically measured M_s is plotted against i/f^2 .

20 As can be seen in Figure 17, the accuracy of a test prototype null-motor balance exceeds 0.1 milligrams.

The final production version of the device should result in a thermocentrifugometric mass analysis having an accuracy in the nanogram range.

25 The speed regulation mode of operation is adaptable for mass measurement processes wherein the centrifugal force generated by the rotating test solid is balanced against a reference force which is independent of the rotational speed.

30 This mode of operation is therefore primarily applicable to the null motor embodiment, the reciprocating shaft null balance embodiment, and the radial displacement embodiment which will be hereinafter discussed. While this embodiment may be used on the angular displacement embodiments, it is
35 not particularly useful inasmuch as the reference weight is subjected to the same centrifugal force field as the test sample. The principle of the speed regulation mode involves

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1 the change in the apparent mass of the test sample by
changing the rotational speed of the device. In both modes
of operation, the centrifugal force generated by the rotating
test sample is balanced against a measurable reactive force
independent from the rotational speed, or:

5

$$\begin{array}{lcl} \text{Centrifugal force} & & \text{Measurable reactive} \\ \text{of test solid} & = & \text{force} \\ \text{proportional to rpm}^2 & & \text{independent of rpm} \end{array}$$

The null force embodiments require two separate
control circuitries, one for the null motor (or the balance
10 beam motor) to generate the reactive force, and the other for
the driving motor to regulate the speed of rotation at a
preselected value. In comparison, only the driving motor
control circuitry is required for the speed regulation mode.
Both modes of operation require a motor with a precisely
15 regulated speed. Synchronous motors are commercially
available with virtually any accuracy desired for
thermocentrifugometric analysis. Many manufacturers state
that their speed regulation accuracies are better than 0.01
rpm at several preselected target speeds in the range of
20 thermocentrifugometric analysis applications. Synchronous
motors, however, require a precision frequency power source
for precise speed control, and this precision frequency power
source is usually quite costly.

DC motors are available with current design and
25 control technologies available that will maintain the speed
regulation within a range of 0.05% under various load
conditions. This corresponds to speed regulation within two
to three rpm at 5000 rpm, and a mass measurement accuracy of
0.1% at 5000 rpm. This level of speed regulation accuracy is
30 felt to be reasonable for most mass measurement purposes of
thermocentrifugometric analyzers in both null mode
environments, and speed regulated modes. The sample control
system for such a motor is set forth in Figure 18 wherein an



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1 adjustable input control signal 640 is used to set the
initial speed of rotation. Speed regulated DC motors are
available commercially with built-in tachometers such as
tachometer 643. This tachometer may be mechanical,
5 electrical, or optical. A variety of commercially available
electronic control circuitries such as 642 are also available
(SCR, SPT, etc.) and are used to provide a regulated current
to the motor 641. The input set speed may be accomplished by
means of an adjustable input control signal 640 which may
10 comprise a potentiometer which bridges a reference voltage
with a tap to the input of the motor controller 642.

In the null motor regulation mode, the operator
only needs to select a potentiometer setting or the
adjustable input control signal 640 to set the rotation of
15 speed and let the controller maintain the speed at that
particular value throughout the entire period of test. On
the other hand, in the speed regulation mode, with the null
force fixed, a control means needs to continuously detect the
displacement and reset the input control signal 640 until the
20 null point is reached. At this point, the rpm is read on
speed display 650. If a constant value of null force is
supplied, and the sample undergoes a change in mass, a
further adjustment of input control signal 640 will be
necessary for each change in mass.

25 Figure 19 illustrates a control circuit for
combining the null force embodiment mode and the speed
regulation mode. The null force mode is equally applicable
to the angularly adjustable null force embodiment illustrated
in Fig. 3, the reciprocating rod embodiment illustrated in
30 Fig. 8, and the radial displacement mode illustrated in Fig.
22. While the precise details of the circuit illustrated in
Fig. 19 will vary from embodiment to embodiment, Fig. 19 will
be explained with reference to the embodiment illustrated in
Fig. 3. In this embodiment, the adjustable initial speed

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1 control signal 640 provides a positive reference voltage e_0
to comparator circuit 644. Simultaneously, the null detector
27e which, as illustrated in Fig. 3 is optical, provides an
output current to conditional converter 644. A conditional
5 converter is used to convert the output current or voltage
from the null detector to a consistent uniform control
voltage for amplifier 645. As illustrated in Figures 2a-2d, a
variety of null detectors may be used to indicate the
rotation of rotor 13 or 13a. Depending upon the type of null
10 detector used, the output may vary, thus requiring the
conditional converter 644, to provide a consistent output
voltage to amplifier 645. The output voltage e_0 is
indicative of the angular displacement of the rotor 13.
Comparator circuit 44 is used to calculate $e_0 - e_\theta$ where
15 e_0 is the null voltage and e_θ is the angular displacement
signal converted to voltage. If e_θ is $> e_0$ (or $e_0 -$
 e_θ is < 0) it means that the rotational speed is too
high, and therefore the voltage input e_p to the driving
motor control circuit has to be reduced in order to lower the
20 motor speed. Amplifier 645 is provided to adjust the
sensitivity of the driving motor control circuit with respect
to the angular displacement signal. Integrator 646 allows
only a small variation in the voltage input ($e_0 - e_\theta$) to
the driving motor control circuit 642. The adjustable
25 initial speed control signal 640 is used to set the initial
rotational speed of the device.

The adjustable initial mass null signal may be a
potentiometer bridged across a reference voltage, with the
tap of the potentiometer providing the initial mass null
30 signal e_0 . The initial mass null signal 647 is set while
the device illustrated in Figure 3 is at rest, to initially
balance the null force generated to the mass of the test
material contained in basket 414 (illustrated in Fig. 15) or
the mass of the sublimating solid 14e illustrated in Figure
35 3.



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1 The voltage input e_p then adjusts the speed of
motor 641 via motor controller 642 in response to the
movement of flag 29e sensed by null detector 27e. The motor
output speed, as determined by tachometer 643, is then fed to
5 conditional converter 647 as illustrated in Fig. 19. The
signal f arriving at conditional converter 647 is
representative of the frequency of motor 641. Inasmuch as
the tachometer 643 can be any commercially available
tachometer, and may provide the signal f in current, voltage,
10 or digital form, a conditional converter 647 is provided to
provide a uniform voltage output that is a square (f^2) for
the speed of rotation of motor 641.

Simultaneously, a reference voltage 649 is divided
by potentiometer 641 and fed to the rotor disk coil 202. The
15 current flow (I) through rotor disk coil 202 is also provided
to divider circuit 648 with the current (I) Supplied as the
enumerator, and signal f^2 as the denominator. The output
of divider circuit 648 is then multiplied by adjustable
amplifier 652 to provide a constant functional value of the
20 output signal from divider circuit 648. The output of
adjustable amplifier 642 is then displayed on a mass display
readout 653.

As was indicated previously with respect to Table
II and in graph 17, the equation for derivation of the mass
25 of the sample may be illustrated as:

$$M_s = K \frac{i}{f^2}$$

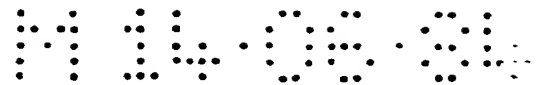
30 In the above equation, the proportionality
constant, K can be calculated from the geometry of the coil
and the magnet field strength from magnets 201, 203. This
constant, K , is provided by adjustable amplifier 652.
However, when the magnetic field is difficult to measure an
35 alternative to the calculation procedure is to determine the
constant K from a linear regression preselected test data.

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1 This was done with respect to the data in Table II to derive
Figure 17.

5 Figures 20, 21 and 22 illustrate the radial
displacement and radial displacement force modes of
operation. As illustrated in Figure 20, the rotor arms 716
and 717 extend outwardly from the rotating shaft at 90
degrees from the shaft. In these embodiments, there is no
second axis of rotation, and the displacement force is
10 generated along a radial axis that is perpendicular to the
axis of shaft 11.

As illustrated in Figure 20, a radial displacement
apparatus is illustrated in a high pressure, high temperature
fluid reactor. A base housing 700 defines a support base for
15 the reactor, the lower half of the reaction chamber 701, and
provides a recess for bearing member 702 which supports the
lower most portion of shaft 11. Base member 700 also defines
a cavity 712 for receiving a drive motor (not shown) to drive
shaft 11. The second half of the reactor, 703, defines the
20 upper portion of reactor cavity 701, and instrumentation
chamber 704 and provides a recess for bearing 705 which
supports the upper portion of shaft 11. As illustrated in
Figure 20, shaft 11 has an enlarged portion 11a which
receives a cantilever beam support 706. Support arms 716 and
25 715 are cantilevered from the vertical support member 706.
Support member 706 is precisely centered in shaft 11a by
means of adjustment screws 707 and 708. The vertical support
member 706 has an elongated vertical member 706a which is
coaxially aligned along the axis of rotation of shaft 11. A
30 strain gauge 709 is mounted on the elongated shaft 706a to
provide an indication of deflection arising from radial
displacement of member 706a by means of the radial
displacement force exerted thereon by rotating test sample
714 and reference weight 715. Strain gauge 709 is connected
35 to preamplifier 710 by means of a cable 711 which passes
through shaft 11. A second cable 712 connects the
preamplifier 710 to a slip ring 713a mounted on the upper end
of shaft 11. The slip ring 713a and slip ring commutator 713b



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1 provide a rotary to stationary connection for the output of
strain gauge 709. The stationary commutator is then
connected to an output terminal 760 for interconnection with
the remainder of the apparatus circuitry. The strain gauge
5 709 may contain a wheatstone bridge circuit, which is
suitable for static strain measurement, and a balance circuit
which is suitable for dynamic strain measurements.
Additional strain-gauge circuitry may also be mounted on the
rotating shaft 11, or in the cabinet housing 761 mounted
10 above rotating shaft 11. The instrumentation chamber 704 is
accessed by means of hatch 762 and is cooled by means of a
gas inlet port 718. The strain gauge and rotating shaft 11
are cooled by air or gas which circulate from inlet ports 719
and 719a to exhaust ports 720a, and 720b which provides for a
15 high speed purging of the high temperature gases present in
the reaction chamber 701. The reaction gases are admitted to
the reaction chamber 701 by means of inlet port 721 and
exhausted by means of exhaust port 722. Close tolerances
that are possible with the radial displacement mode permit a
20 centrifugally outward sweep of gas through the annular
passageway 723. A thermocouple wall 724 provides a means for
monitoring the temperature of the reaction chamber. An
electrical heating means 725 and 726 provide means for
heating the interior of the reaction chamber 701 to
25 temperatures as high as 2500 degrees. A solids loading port
727 is provided in the upper portion of the support member
703 and is capped by means of plate 728.

As illustrated in Figure 20, when the device is at
rest, the solids container 714, which may assume the
30 configuration of the container illustrated in Figure 10, is
loaded through access port 27. The device is then rotated to
provide for the adjustment of reference weight 715 to
statically balance the cantilever beam. As the device is

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1 rotated, the sample receiving means 714 is displaced upwardly
as illustrated in Figure 20, as the device achieves a
preselected initial operating speed. After the desired
rotational speed has been reached, the reaction study is
5 begun by heating the autoclave chamber 701 by means of
electrical resistance heating means 725 and 726, and then
admitting the desired reaction gas through port 721. As the
sample in the sample receiving means 714 undergoes a change
in mass, the net change is reflected in a dynamic unbalance
10 of the mass on rotor arms 715 and 716. This unbalance is
then measured by strain gauge 709 and a ballast circuit to
provide a derivative value of the change in mass, as
amplified by the centrifugal force generated by the
thermocentrifugometric analyzer.

15 In the apparatus illustrated in Figure 21, the
support members 840 and 842 define recesses for bearings 841
and 843 which support shaft 11 for rotation. In between
support members 740, 742 is a quartz reactor tube 844 which
defines an annular cylinder 844a and a toroidal reaction
20 chamber 844b interconnected with the cylindrical member 844a
by means of an annular chamber 844c. The quartz reaction
chamber defines a gas inlet port 845 and a gas exhaust port
846 for admission of preselected reaction gases. A solids
loading port 847 is also defined at one portion of the
25 reactor tube. In operation, ports 845 and 846 are connected
to a supply and exhaust of the desired reaction gas, and port
847 is capped during the reaction period. An instrumentation
chamber 748 also defines an inlet port 849 for the admission
of cooling air. The configuration of shaft 11 is somewhat
30 different than that previously described with respect to
Figure 20. The solid sample holder 814 is suspended from
support arm 816 which is pivotably mounted to a support
member 817 mounted along a 90 degree radial axis with respect
to the axis of rotation of shaft 11. Member 817 is mounted
35 on a load cell 818 which is secured to shaft 11 by nut 819 on
the other side of support web 720. While member 817 does not
visually reciprocate, it does



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1 reciprocate to the extent necessary to transmit the
displacement force generated by the rotating test sample and
test sample receiving means 814 to load cell 818 as the
sample undergoes a change in mass. A rotating vane and
5 radiation shield 821 is connected between load cell 818 and
reaction chamber 844b. Diametrically opposed to rotating
vane and shield 821 is a second vane 822 which may also
contain a reference weight to offset the mass of support arm
816 and sample receiving means 814. This enables the shaft
10 to be dynamically balanced, except for the size of the sample
placed in the sample receiving means 714.

Load cell 818 may be of several different types.
The reciprocal displacement is extremely small. For example,
strain gauge load cells involve only a fraction of a
15 thousandth of an inch of reciprocal movement. The linear
variable differential transformer load cells involve larger
displacements and may require additional force compensation.
A typical load cell for use in a device as illustrated in
Figure 21 is the ELF-1000 series flat line load cell
20 manufactured by Entran Devices Inc., 10 Washington Avenue,
Fairfield, N.J. 07006. These load cells have a self
contained wheatstone bridge, whose output is transmitted
along cable 825 to compensation module and preamplifier
circuit 826. The output of the preamplifier 826 is fed to a
25 rotating commutator rings 827 and thence to the stationary
slip ring 828 for connection to the outside of the
instrumentation chamber as indicated by terminal 829. The
quartz reaction chamber 844b is heated by means of radiant
heaters 830 which surround the torroidal portion of the
30 quartz reaction chamber.

The apparatus illustrated in Figure 22 is similar
in many respects to the apparatus illustrated in Figure 21.
A quartz reaction chamber is suspended between a lower
support or base member 840 and an upper support or base

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1 member 842. However, the toroidal portion of the quartz
reaction chamber is surrounded by an induction coil 831 for
inductively heating the sample contained in the rotating
sample receiving means 714. With the exception of the load
5 cell and reciprocating apparatus mounted in rotating shaft
11, the remainder of the device is identical to the apparatus
illustrated and described with respect to Figure 21. A
reciprocating shaft member 832 is mounted for reciprocation
in shaft 11 and has attached thereto support arms 716 and
10 717. Support arms 716 supports the solid sample receiving
means 714 and rotating arms 717 supports the reference weight
715. The load cell and shaft 11 are protected from the
intense heat and/or radiation present in the annular chamber
844 by means of the baffles and radiation shields 833 and
15 834. These create a purging outward centrifugal flow of gas
from the cavity surrounding shaft 11 to the angular reaction
chamber 844. Attached to piston 832 is a reciprocating disc
835 which is biased into engagement with a load cell 836 by
means of spring means 837. The spring means 837 is retained
20 in position against the reciprocating disc 835 by means of a
threaded nut 838 which is externally threaded to engage the
threads 839 defined on the interior walls of the recess of
shaft 11.

In operation, the sample receiving means 714 is
25 loaded through the solids loading port 747, and the device is
statically balanced by means of weight 715 by rotating shaft
11 to bring the reference weight 715 into alignment with the
solids loading port 747. After the device is statically
balanced, the initial rotational speed of the device is
30 selected, and a variable speed DC motor mounted in recess
712, is used to drive shaft 11 to its preselected operating
speed. The load cell 836 is compressed by means of the
radial force generated by the sample and sample receiving
means 714, and transmits the output of its wheatstone bridge
35 to preamplifier 826. The output of the preamplifier is



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1 transmitted by means of the commutator ring 827 to the output
terminal 829. Spring means 837 provides a positive loading
for load cell 836, even if the sample received in the sample
receiving means 714 is reduced to zero mass.

5 Each of the principal embodiments previously
illustrated with respect to Figure 1, 7, 8, 13, 14, 15, 16,
18, 19 and 20 disclose an angularly extending arm having a
basket suspended therefrom for receiving a test sample to be
measured. Figure 10 describes an alternate embodiment of the
10 sample holding means wherein the basket 13 is replaced with a
unique solids container 111.

The test samples to be measured may come in a
variety of sizes ranging from large particles to very fine
powders. For big particles, a loosely woven basket such as
15 that illustrated in Figure 1 is quite satisfactory since the
weave, in comparison to the size of the tested particles,
allows the fluid or gas to pass freely between the solids.
The basket configuration however is not satisfactory for very
fine powders because even a small layer of such powders would
20 force the fluid to deflect and pass around the container. In
the example illustrated in Figure 10, the fluid path 112 to
be impinged upon the test sample to be analyzed is directed
at the solids container 111 to enter the mouth 113 of the
container. The solids container 111 has drilled therein a
25 duct 114 illustrated by the dotted lines in Figure 10. The
duct terminates in a discharge screen 115 which is secured to
the solids container 111 by welding or by means of plate 116
and a plurality of screws, one of which is illustrated on
117. The fluid flow through the duct 114 can be further
30 increased by placing an air foil at the discharge end, or by
making the diameter of the mouth 113 (D_m) somewhat larger
than the diameter of the discharge exit 118 (D_2).

The unique solids container described in Figure 10
provides a modified Froessling equation for gas-solid mass
35 transfers:

$$Sh = 2.0 + 1.80 Sc^{1/3} Re^{1/2}$$

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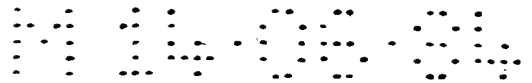
1 The effects of film mass and heat transfer
resistances on the observed gas-solid reaction rate
measurements are well known. For first order irreversible
reactions, the observed reaction rate is given by:

5

$$R_A = \frac{P_{Ag}}{\frac{1}{k_g} + \frac{1}{k_s}}$$

10 In which R_A is the rate of disappearance of gas A
per unit surface area of solid, P_{Ag} is the measurable and
controllable bulk gas particle pressure of A, k_g is the film
mass transfer coefficient, and k_s is the reaction rate
15 constant measured on the surface of the reacting solid. In
order for the observed reaction rate to represent the true
reaction mass under both mass conditions, it is necessary
that the mass transfer coefficient be much greater than the
surface reaction rate constant, or $k_g \gg k_s$ and that the
20 surface temperature of the solid be identical to the bulk gas
temperature. This requires that the gas and solid be
contacted at sufficiently high velocities. In the present
invention, a gas transfer rate of 40 meters per second may be
achieved at 4000 rpm. This high sweep gas rate may be
25 achieved in a unique high temperature quartz reaction chamber
at temperatures in excess of 1500 degrees. Even higher sweep
rates can be used with operating speeds as high as 10,000
rpm.

Figure 12 describes the cross section of a unique
30 quartz reaction chamber for use in the thermocentrifugometric
analyzer. As illustrated in Figure 12, the reaction chamber
includes a central cylindrical portion 744a, a toroidal
member 744b which surrounds the cylinder, and an annular
chamber member 744c. The toroidal member 744b defines a
35 reaction chamber 744 for high temperature reaction studies.
The device is particularly adapted to radiant heat studies
wherein a radiant heater 760 is placed around the quartz tube



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1 744b. An inlet port 745 is formed on one side of the device,
and an exhaust port 746 is formed on the opposite side of the
toroidal cavity 744. Inlet 745 and exhaust 746 are used for
admission and exhaust of the reaction gas introduced into
5 chamber 744. A solids loading port 747 is formed on one side
of the toroidal cavity 744. This solids loading port is
normally capped with a cap 747a as illustrated in Figure 12.
Gas is normally introduced into the central cavity 744d to
provide a purging and cooling gas flow for the rotating shaft
10 and circuitry installed on rotating shaft 11. If desired,
O-rings 780 and 781 may be used to seal the quartz reaction
chamber. During operation, gas is normally introduced into
cavity 744d at pressures up to 2 psig to radially displace
the air flow towards the reaction chamber 744. In addition,
15 the rotation of shaft 11 and of the rotor arms 716 and 717
will cause a radial outflow of the air through the annular
passageway defined at 744c.

An alternate reaction chamber is disclosed at
Figure 9. Figure 9 illustrates diagrammatically, a means
20 that may be installed in an autoclave chamber to assist in
gas-solid reaction studies.

The rotation of shaft 11 and basket 114 may induce
a whirling motion of the gaseous reaction media, however, a
stationary gas is desirable. One means for inhibiting
25 whirling motion and continuing the gas motion to a radial
motion rather than a circumferential motion is disclosed in
Figure 9. The primary mechanism of gas mixing in the reactor
is displacement mixing. It utilizes a percolating gas flow
through the rotating container 114. When the device
30 illustrated in Figure 9 is used for the mixing, the
calculations show that the displacement flow, occurring in the
direction of rotation G, but without creating any significant
gross whirling motion of gas, will amount to rpm x active
displacement volume for each container summed over all of the
35 chambers 765, or $4000 \times 0.2 \times 2 = 1600 \text{ cm}^4/\text{minute}$ for the

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1 apparatus and container shown in Figure 9 when rotating at
4000 rpm. When the angular momentum of the displacement gas
is discharged from the rotating container is mechanically
dissipated by means of the appropriately spaced baffles 761,
5 the gas flow pattern in the reaction chamber will be much
like the cross recycle flow pattern illustrated by arrows 766
and 767.

The normal rotation of the solid sample receiving
means 114 as illustrated in Figure 9 causes a circumferential
10 and centrifugal movement of the gas along the direction of
arrow G illustrated in Figure 9. By placing an annular
baffle ring immediately outside the circumferential path of
the sample receiving means 114, the gaseous fluid is directed
outwardly rather than circumferentially. As was indicated in
15 Figure 10, the solid receiver 114 has an inlet opening 113
and an exhaust opening 118 the rotation of the solid receiver
114 forces the gas into port 113 and out of exhaust port 118.
The series of radial baffles 761 are positioned around the
axis of rotation of shaft 11. The distance between the
20 baffles is determined by the following formula:

$$\text{baffle distance} = \frac{(\text{container length}) - (\text{circulation velocity})}{(\text{percolation velocity})}$$

25

The radial baffles 761 are secured by a pair of
annular plates, one of which is illustrated as 762 in Figure
30 9. The height of the baffles 761, and the spacing of the
annular plates 762 and 763 (not shown) is determined by the
size of the solids container 114. In operation, the reaction
gas is emitted through port 764 and discharged through port
765.

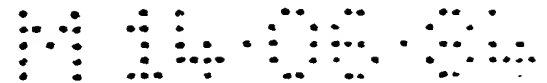
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1 Perfect mixing of the gas is essential in order to
operate the thermocentrifugometric analyzer as an integral
mixed flow reactor. This insures uniform bulk gas
composition throughout the entire reactor gas space without
5 using extensively large gas throughput rates. The gas mixing
in the reactor is primarily dependent on the displacement
flow of the gas produced by the rotating container 114, in
the direction of the arrow G.

Figure 13 discloses another alternate arrangement
10 for measuring the angular displacement of rotor 13 in a
thermocentrifugometric mass analyzer. As illustrated in
Figure 13, the rotating shaft 11 is powered by means of a
variable speed drive motor 12 to rotate baskets 14 and 15
about a first axis of rotation A-A'. The shaft 11 is secured
15 by a thrust bearing 135 and the autoclave chamber is sealed
at 136 and 136a to prevent the escape of high temperature,
high pressure gas. The gas may be admitted into the
autoclave 40 by means of inlet 61 and exhausted through
conduit 62 as has been previously described with respect to
20 Figure 2. A cooling chamber 136 is provided to insulate the
autoclave from the driving and support mechanisms.

In the device illustrated in Figure 13, an optical
readout means is provided wherein a light source or any other
radiant energy source 137 is positioned directly above rotor
25 13 and projects a beam of radiant energy 138 downwardly along
axis A-A' through a quartz lens 144. An optical reflector
means 139 is formed in rotor 13 to substantially deflect the
beam of light or radiant energy from axis A-A' to a
perpendicular axis indicated at 140. A quartz window 141 is
30 provided in the wall of autoclave 40 with a series of
photodiodes or other radiant energy responsive devices 142
arranged on the exterior of the autoclave chamber adjacent



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1 the quartz window. During operation of the device, the
angular rotation of disc 13 causes a vertical displacement
H-H' of the beam of radiant energy 140. As the beam or light
ray sweeps past the quartz window 141, it energizes one of
5 the photodiodes or other light sensitive devices 142 arranged
on the exterior of the autoclave. The area energized is then
converted into a measurement indicative of the angular
displacement of rotor 13 by display device 143. Alternately,
the value of the change in mass for the sample and container
10 14 may be calculated and displayed.

An alternate placement for light source 137 is
indicated by dotted lines 137a in Figure 13 wherein the light
beam or beam of radiant energy is projected downwardly
through a quartz lens 144a into the autoclave chamber 40. A
15 portion of the support arm 16 designated at 145 is provided
with a reflective device to reflect the light beam 138a
through the quartz window 141 to strike the photodiode array
at 142a. In this embodiment, an alternate compensating
weight is added at 146 on the support arm 17. In each case,
20 the device generates a single pulse of light on the
photodiode array 142 for each revolution of shaft 11. The
angular displacement of the beams 140 and 140a provide a
derivative value of the change in mass in M_g as the sample
is subjected to preselected temperature and fluid variables.

25 Figures 15 and 16 illustrate the use of the
embodiments previously described with respect to Figure 3 and
8 and a high temperature autoclave environment. Both devices
are "null" type devices involving very little angular
displacement of the rotors inasmuch as any angular
30 displacement is immediately compensated for by a compensating
restoring force.

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1 As illustrated in Figure 15, a high temperature
autoclave 430 is constructed with an annular autoclave
chamber 431 which is heated by means of electric heating
coils 432. For extremely high temperature applications the
5 container hangers 414a, 415a may be extended for increased
thermal isolation of the gas chamber 431. In addition, if
desired, the electrical heating means 432 may be replaced by
an externally mounted radiation heating means with its
thermal radiation focused along the circulation path of the
10 container 414. The autoclave chamber is also supplied with a
gas or fluid inlet conduit 433, and a gas or fluid outlet
conduit 434. A thermocouple well 435 extends from above the
cabinet 430 into the annular reaction chamber 431.

 As was indicated previously with respect to Figure
15 3, shaft 411 rotates rapidly with a reference weight M_r in
basket 415 and a sample M_s in basket 414. Compensator
weights 420 and 421 compensate for the rotor and provide
rotor balance calibration weights. The rotor 413 rotates
about r_o upon a change in mass in M_s carried by basket
20 414. This rotation is detected by means of photo-sensor 466
carried within transducer 427, as flag 429 moves from its
center nulled position. As the photo-sensor 466 generates a
control signal, the control signal is passed by means of
rotating slip ring commutator 405 to the stationary slip ring
25 commutator 404 to the control circuitry illustrated at 436.
The control circuitry then energizes either coil 402 or 403,
or both to generate a restoring force to return rotor 413 to
its central nulled position wherein each of the arms 416 and
417 are equally aligned along the axis of rotation of shaft
30 411. Shaft 411 is journaled for rotation bearings 438 - 439
to provide for high speed rotation of the rotor arms 416 and
417. As was indicated previously with respect to Figure 1,

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1 the speed of rotation may be several thousand rpm. In
addition, the temperatures generated in the high temperature
autoclave may be as high as 2,500 degrees. Cooling coils
generally illustrated at 442 totally surround shaft 411 and
5 411a, and rotor 413 to insulate and cool the operating
structure from the intense temperatures generated in the
autoclave chamber 431. In addition, the reflective and
insulated means 424 previously described with respect to
Figure 6, radiate the heat back towards the annular autoclave
10 chamber 431. In addition to the coolant circulated through
the coils 442, the shaft 411 may be cooled from the interior
by means of coaxial conduits 443 and 444. In this
embodiment, the annular conduit 444 provides a coolant inlet,
while the center conduit 443 provides an outlet for the
15 coolant.

The amount of current supplied to coil 402 and/or
coil 403 to restore rotor 413 to a centered null position is
then converted to a numerical display at 437 that may provide
an indication of the change of weight in M_s as it is
20 reacted with the gaseous or fluid medium in the high
temperature autoclave 431. The display for 437 may be an
absolute or a functional value as desired.

The remainder of the interior within cabinet 430 is
filled with insulation as indicated at 450.

25 The application of the "null" balance beam device
to a high temperature autoclave environment is illustrated in
Figure 16. An autoclave cabinet 530 is used to house an
annular high temperature autoclave chamber 531, and provides
support bearings 538 - 539 for the rotating shaft 511.
30 Rotating shaft also has support vanes 562 and 563 and an
angularly displaceable arm 519 which rotates about pivot
point 564 in the same manner as was described with respect to
Figure 7. The angular displacement of arm 519 caused by a

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1 change in M_s placed in basket 514 is translated into
vertical, reciprocal movement of reciprocating shaft 520.
The vertical force is translated by means of platter 524 to
the balance beam 521 in the same manner as was previously
5 described with respect to Figure 7. The control apparatus
for Figure 16 is the same as was illustrated with respect to
Figure 8. A null balance is preferred for the high
temperature autoclave, inasmuch as it is desired to isolate
the high temperature autoclave chamber 531 from the
10 instrumentation chamber 570 as much as possible. For
extremely high temperature applications the container hanger
514a may be significantly extended for increased thermal
isolation. As was previously indicated with respect to
Figure 8, the balance beam 521 exerts a counter force on
15 reciprocating shaft 520 to maintain the arm 519 in a constant
angular displacement. Forces acting on balance beam 521 may
be generated by the null point gravimetric balance device
550, the compression type null device 552, a rotational motor
551, or a linearly adjustable weight 544. The displacement
20 of the balance beam 521 may be measured by the transducer 527
with respect to the metal or magnetic chip 529, or by the
rotation of a rotational transducer 551 that measures the
rotation of balance beam 521 about axis 526. As was
previously indicated with respect to Figure 8, electric,
25 hydraulic or pneumatic devices may be used to generate the
various forces on balance beam 521. Attached to vanes 562
and 563 are radiation shields 571 and 572 which may also be
configured to provide maximum agitation of the gas or fluid
in the high temperature autoclave chamber 531. High
30 temperature fluid or gas is emitted through inlet port 533
and exited through exit port 534 during the reaction study.
Or if desired, a given amount of reaction product may be
introduced into the chamber 531, and the ports 533 and 534

35

1 sealed for the reaction. If desired, the rotating shaft 511
and the instrumentation
chamber 570 may be insulated by cooling coils as was
previously illustrated with respect to Figure 15. The
5 remainder of the chambers, however, are filled with
insulation 550. If desired, the balance beam device
illustrated in Figure 16 may also be equipped with a
conventional gravimetric scale 583 which is attached to
balance beam 521 by means of cable 584 which passes through
10 ports 580 and 581 and tubular member 582.

While the foregoing application has described a
process and several distinctly separate mechanical devices
for carrying out the process substantial variations in the
details of the specific embodiments it should be apparent
15 that the teaching and disclosure of the present invention
will suggest other embodiments and variations to those
skilled in the art. Many mechanical, optical, electrical,
and electromechanical transducer devices are present that
could be readily adapted or modified for the present
20 invention to provide indication of the angular rotation of
the rotor means 13, or the angular force generated by the
rotor means in the null motor apparatus or the beam balance
apparatus. One specific set of calculations has been
included for test apparatus constructed and used in the
25 determination of the change in mass of a test specimen
subjected to elevated temperatures. The inclusion of the
formulas as herein is not intended in any way to claim or
restrict the use of the mathematical formula to applicant's
invention, but is intended to teach those skilled in the art
30 how to use applicant's invention to design centrifugometric
mass analyzers capable of handling a variety of solid sizes
in a variety of ambient operating conditions.

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WE CLAIM:

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1. A method for measuring a change in mass of a test sample when the sample is subjected to selected temperature and fluid variables, said process comprising:

10

- (a) rotating a test sample about an axis to subject the sample to centrifugal force;
- (b) subjecting the test sample to a selected temperature and fluid to effect a change in mass of the test sample;
- (c) measuring a displacement or a displacement force generated during the rotation of the test sample to determine a change in mass during an interval of time;

15

whereby any change in mass in the test sample may be measured by a derivative value of the displacement or displacement forces generated at the beginning and end of said time interval.

20

2. A method for measuring a change in mass of a test sample as claimed in claim 1 wherein the displacement of the rotating test sample is measured to obtain a derivative value of the mass of the samples.

25

3. A method for measuring a change in mass of a test sample as claimed in claim 1, wherein the displacement force generated by the rotating test sample is measured to obtain a derivative value of the mass of the sample.

30

4. A method for measuring a change in mass of a test sample as claimed in claim 1 or 3 wherein the speed of rotation is varied to balance the displacement force generated by the test sample against a known reactive force.

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5. A method of measuring a change in mass of a test sample as claimed in claim 1 or 2 which further includes the step of suspending the test sample from a rotatable means, said means having a second axis of rotation perpendicular to the axis of rotation in step (a), and measuring a displacement about the second axis of rotation.

10

6. A method for measuring a change in mass of a test sample as claimed in 1 or 3 or 4 or 5 which further includes the step of generating a reactive force to balance the displacement force generated by the rotating test sample, and then measuring the reactive force.

15

7. A method for measuring a change in mass of a test sample as claimed in claim 1 or 2 or 3 or 4 which further includes the step of measuring the displacement force with a transducer means positioned between the test sample and the axis of rotation.

20

8. A method for measuring a change in mass of a test sample as claimed in claim 1 or 2 or 5 or 6 which further includes the steps of:

(a) placing the test sample in a displaceable sample receiving means;

25

(b) balancing the test sample receiving means with a known reactive force before said sample is rotated.

30

9. A method for measuring a change in mass of a test sample as claimed in claim 8 wherein the known reactive force is generated by a reference weight before the test sample is rotated.

35

10. A method for measuring a change in mass of a test sample as claimed in claim 7 or 8 or 9 which further includes the step of generating one or more compensating forces to compensate for one or more rotating elements.

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11. A method for measuring a change in mass of a test sample as claimed in claims 1 or 2 or 3 or 4 or 5 or 6 or 7 wherein the change in mass is continuously measured.

5

12. A method for measuring a change in mass of a test sample as claimed in claim 1 or 2 or 3 or 4 or 5 or 6 wherein the change in mass is adapted to be measured by a differentiated value of displacement forces at the beginning and end of at least one finite interval of time.

10

13. A method for measuring a change in mass of a test sample as claimed in claim 1 or 3 or 4 or 5 or 6 which further includes the step of varying at least one adjustable force element to balance the displacement force generated by the test sample.

15

14. A method for measuring a change in mass of a test sample as claimed in claim 13, which further includes the step of simultaneously varying the speed of rotation and at least one adjustable force element to balance the displacement force generated by the test sample.

20

15. A method for measuring a change in mass of a test sample as claimed in claims 1 or 3 or 4 or 5 or 6 which further includes the step of generating a reactive force to balance the displacement force with a variable beam balance.

25

16. A method for measuring the change in mass of a test sample as claimed in claim 1 or 2 or 3 or 4 or 5 or 6 which further includes the step of rotating the sample receiving means between 200 rpm and 5000 rpm.

30

17. A method of measuring the change in mass of a test sample as claimed in claim 16, which further includes the step of directing a high velocity gaseous fluid against the test sample as it is rotated.

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18. A method of measuring the change in mass of a test sample as claimed in claim 1 or 2 or 3 or 4 or 5 or 6 which further includes the steps of:

5

(a) rotating the sample at a speed of at least 200 rpm;

(b) elevating the temperature of the ambient atmosphere surrounding the sample to a preselected temperature.

10

19. A method of measuring the change in mass of a test sample as claimed in claim 18 which further includes the step of surrounding the sample with a preselected fluid.

15

20. A method of measuring the mass of a test sample as claimed in claim 19, which further includes the step of suspending the solid sample for rotation and sublimating it by a reaction with a preselected fluid.

20

21. A thermocentrifugometric analyzer for measuring the mass change of a test material subjected to selected temperature and fluid variables, said analyzer comprising:

25

(a) a rotating shaft and means for rotating said shaft around a first axis of rotation;

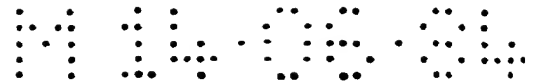
(b) a test material holding means extending outwardly from said shaft to hold a test material while it is rotated about said axis of rotation;

30

(c) an enclosure means for subjecting the test material to preselected temperature and fluid variables to effect a change of mass of said sample;

35

(d) a means for measuring a displacement or a displacement force generated by said test material holding means when said test material is rotated about said axis of rotation and is subjected to selected temperature and fluid conditions.



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1 22. A thermocentrifugometric analyzer as
 claimed in claim 21, wherein said means for measuring
 the displacement force further comprises a means for
 generating a null force to balance a displacement force
5 generated by the rotating sample, and means for measuring
 the magnitude of the null force generated.

 23. A thermocentrifugometric analyzer as claimed
 in claim 21, wherein said analyzer further includes a
 means for measuring the displacement force generated
10 by the test sample at selected points in time as it is
 rotated.

 24. A thermocentrifugometric analyzer as claimed
 in claim 21 wherein said test material holding means is
 pivotably mounted on said shaft to rotate about a second
15 axis of rotation, said second axis of rotation being
 perpendicular to said first axis of rotation.

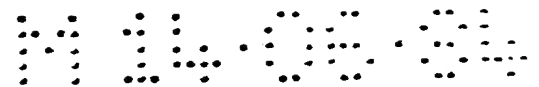
 25. A thermocentrifugometric analyzer as claimed
 in claim 24, wherein said analyzer further includes a
 reference weight to balance said sample about said second
20 axis of rotation before said shaft is rotated.

 26. A thermocentrifugometric analyzer as
 claimed in claim 21, wherein said means for measuring
 the displacement force comprises a balance beam.

 27. A thermocentrifugometric analyzer as claimed
25 in claim 21, wherein said analyzer further includes a
 means for varying the speed of rotation of said shaft
 and said test sample.

 28. A thermocentrifugometric analyzer as
 claimed in claim 21 or 23, wherein said measuring means
30 further comprises a load cell.

 29. A thermocentrifugometric analyzer as claimed
 in claim 23 or 28, wherein said analyzer further includes
 a reference weight mounted to generate an opposing
 linear displacement force as said shaft is rotated.
35



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1 30. A thermocentrifugometric analyzer as
claimed in claim 21 or 23, wherein said analyzer further
includes a strain gauge mounted on said rotating shaft
for measuring displacement force transmitted by said
5 holding means to said rotating shaft.

 31. A thermocentrifugometric analyzer as claimed
in claim 26, wherein said balance beam initially balances
the test material and holding means while
rotating , said analyzer also having a control
10 means for maintaining a dynamic balance of said apparatus
with a variable null force to offset a change in the
displacement force generated by the rotating test material,
whereby any change in mass, over time, will be measured
as a derivative value of the magnitude of the null
15 force generated.

 32. A thermocentrifugometric analyzer as
claimed in claim 21 or 22 or 26 or 27 or 30, wherein
said analyzer further includes a reference weight to
balance said sample before said shaft is rotated.

20 33. A thermocentrifugometric analyzer as
claimed in claim 21 or 22 or 27, wherein said analyzer
further includes a reference mass to be rotated and
thereby offset the force generated by the mass of said
test material holding means.

25 34. A thermocentrifugometric analyzer as
claimed in claim 27, wherein the means for rotating
said shaft at variable speeds is responsive to said
means for measuring the displacement force;

 whereby the displacement force generated by
30 the test sample is maintained at a constant value as
the speed of rotation is varied.

 35. A thermocentrifugometric analyzer as
claimed in claim 31, wherein said analyzer further
includes a means for varying the speed of rotation of
35 said shaft to rebalance said test sample to said
reference weight as said test material undergoes a
change in mass.



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1 36. A thermocentrifugometric analyzer as
claimed in claim 21 or 22 or 23 or 26 or 27, wherein
said sample holding means is connected to said shaft
by an outwardly extending arm.

5 37. A thermocentrifugometric analyzer as
claimed in claim 24 or 25, wherein said analyzer further
includes a compensator means mounted on a support means
to compensate for the rotating mass of said test material
holding means.

10 38. A thermocentrifugometric analyzer as
claimed in claim 21 or 23 or 27, wherein said analyzer
further includes a cantilever beam mounted on said
rotating shaft, said cantilever being supported by a
15 first beam having a center axis aligned along the axis
of rotation of said shaft, with said cantilever beam
supporting said test material holding means, said
analyzer also including a strain gauge mounted on
said first beam for measuring said linear displacement
20 force by measuring forces transmitted to the first
beam by said cantilever beam.

39. A thermocentrifugometric analyzer as claimed
in claim 21, which further comprises:

25 (a) a means for generating a null force to
offset a change in displacement force generated by
the rotating test material;

 (b) a means for varying the null force in
response to a change in displacement force and a means
for generating a null signal representative of the applied
null force;

30 (c) a means for varying the speed of rotation to
vary the magnitude of the displacement force generated
by the test material and a means for generating a signal
representative of the speed of rotation;

35 (d) a means for measuring the mass of the test
material as a value derived from the displacement force
signal and the speed of rotation signal.

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1 40. A thermocentrifugometric analyzer as
claimed in claim 39, wherein said analyzer further includes
a reference weight of known mass to effectively increase
or decrease the range of mass measurement.

5 41. A thermocentrifugometric analyzer as claimed
in claim 21 or 22 or 24 or 26 or 27, wherein said analyzer
further includes an annular chamber surrounding a rota-
tional path defined by said test material, said annular
chamber having a series of radial baffles therein for con-
10 verting circumferential flow of said selective fluid
into a series of radial flow patterns.

 42. A thermocentrifugometric analyzer as claimed
in claim 21 or 22 or 24 or 26 or 27, wherein said test
material holding means further includes a solid sample
15 holder for receiving said test material, said sample
holder having a first inlet opening oriented in the
direction of rotation, a second outlet opening oriented
along a radial axis when said analyzer is rotating, and
means for retaining a solid test sample adjacent said
20 second outlet opening.

 43. A thermocentrifugometric analyzer as claimed
in claim 21 or 22 or 24 or 26 or 27, wherein said analyzer
further includes an annular reaction chamber, an autoclave
surrounding said reaction chamber, and means for intro-
25 ducing a preselected fluid into said reaction chamber.

 44. A thermocentrifugometric analyzer as
claimed in claim 43, wherein said annular reaction
chamber is formed of glass or quartz.

 45. A thermocentrifugometric analyzer as claimed
30 in claim 21 or 22 or 24 or 26 or 27, wherein said enclosure
means for subjecting the test material to preselected
temperature and fluid variables further comprises:

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- 1 (a) a means for admitting at least one
preselected fluid;
- (b) a means for withdrawing the preselected
fluid;
- 5 (c) a heating means;
- (d) a means for measuring the temperature of
the fluid at least at one point in the enclosure space;
- (e) a control means responsive to the temperature
measuring means for raising or lowering the temperature
10 in a predictated manner and maintaining the temperature
at a desired value.

46. A thermocentrifugometric analyzer as claimed
in claim 21 or 23 or 27 or 29 or 30, wherein said enclosure
comprises of an outer annular chamber surrounding a
15 rotational path defined by said test material, an inner
chamber surrounding the rotating shaft, and a middle disc
like space connecting said inner chamber to said outer
chamber.

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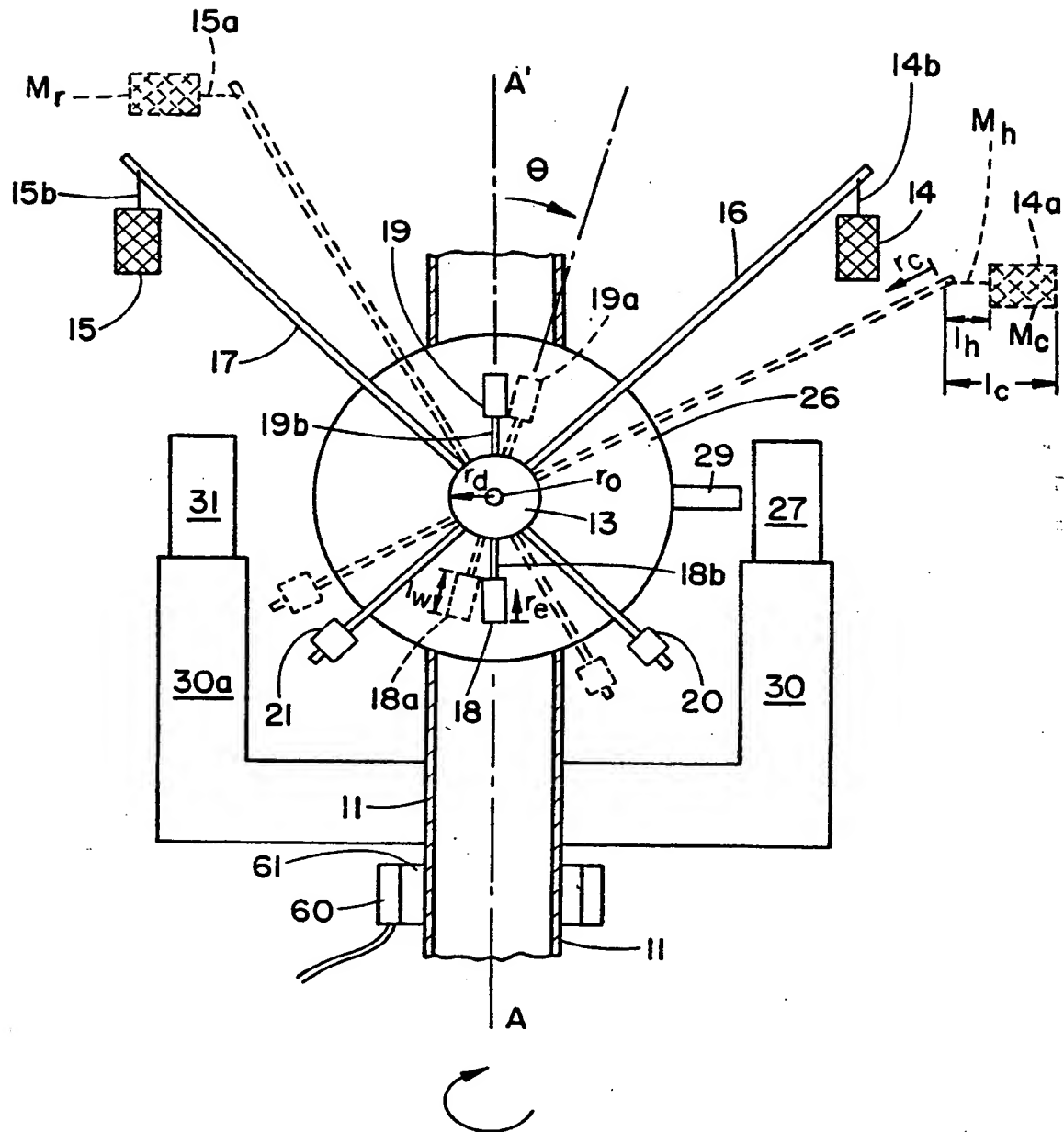


FIG. 1

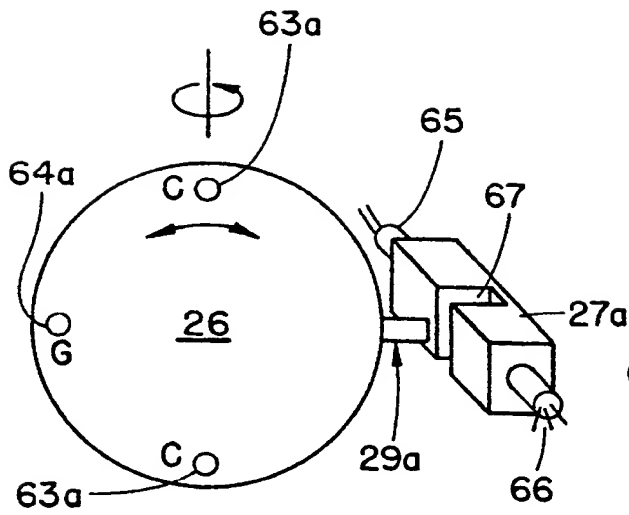


FIG. 2a

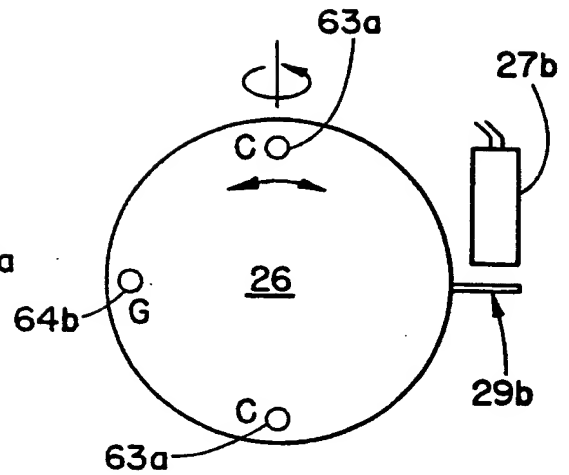


FIG. 2b

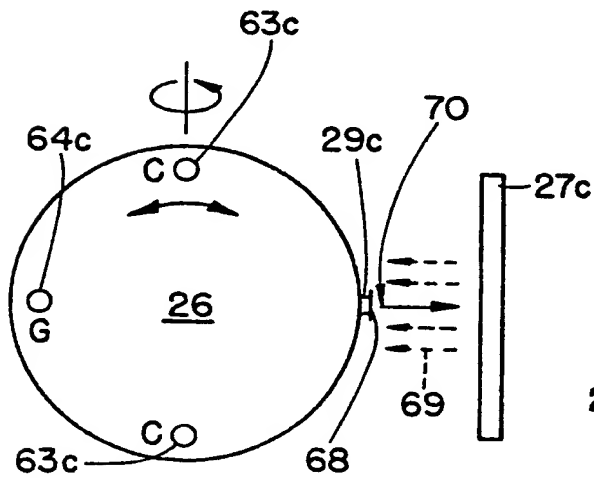


FIG. 2c

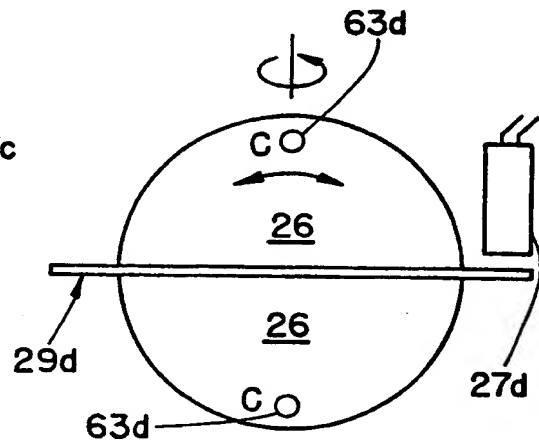
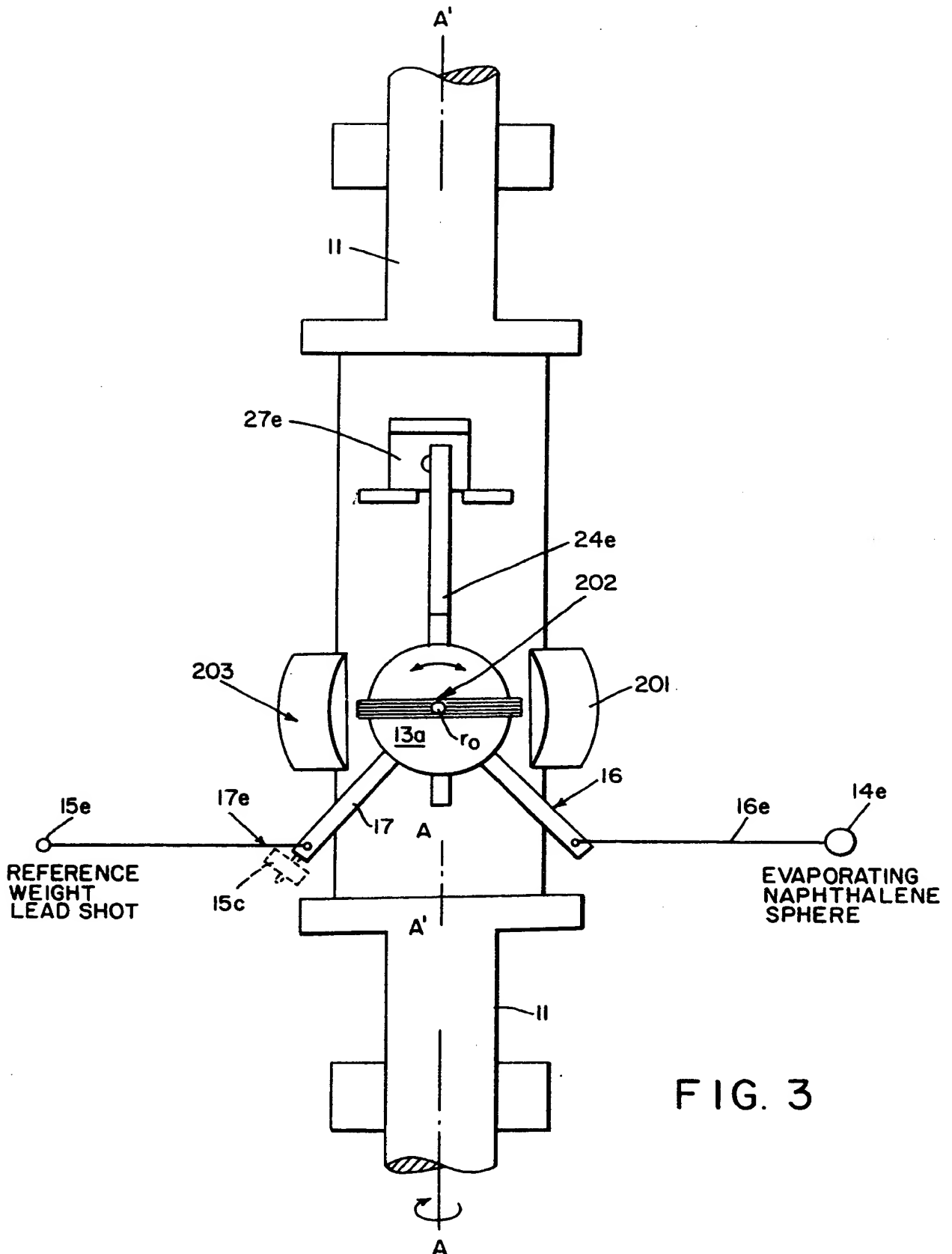


FIG. 2d



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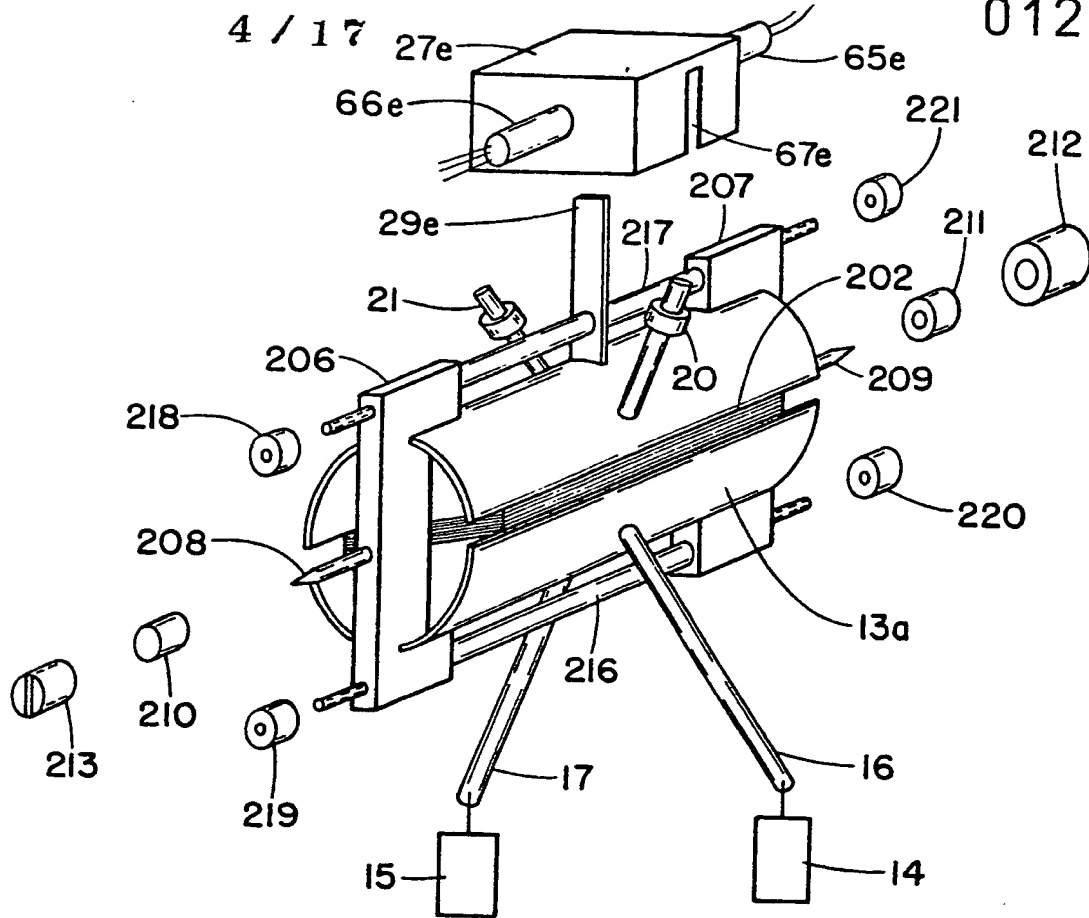


FIG.4

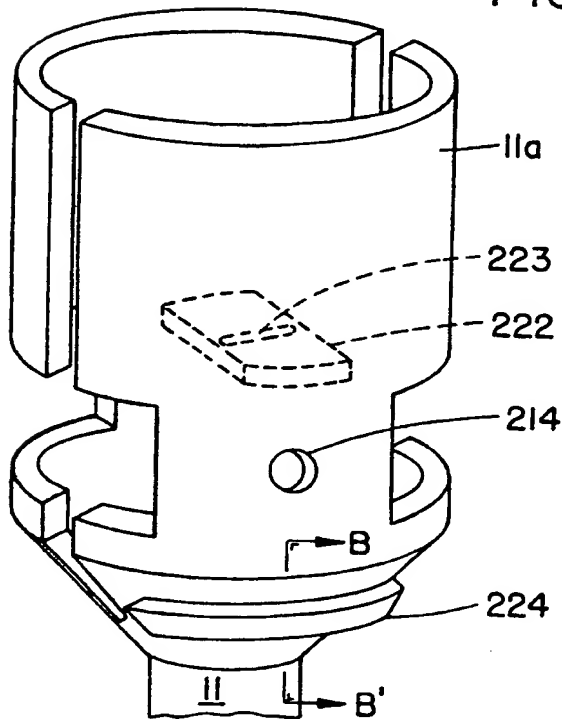
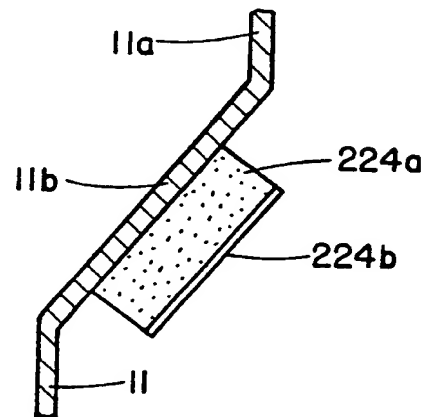


FIG.5





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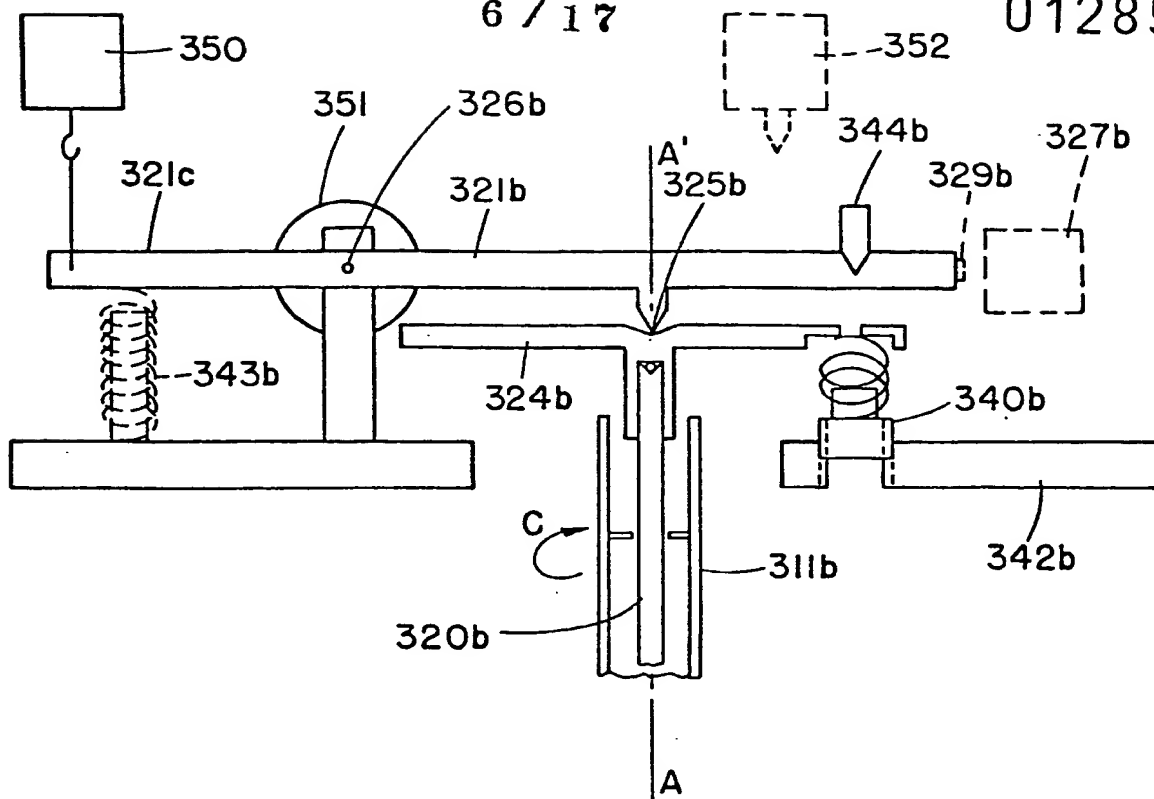


FIG.8

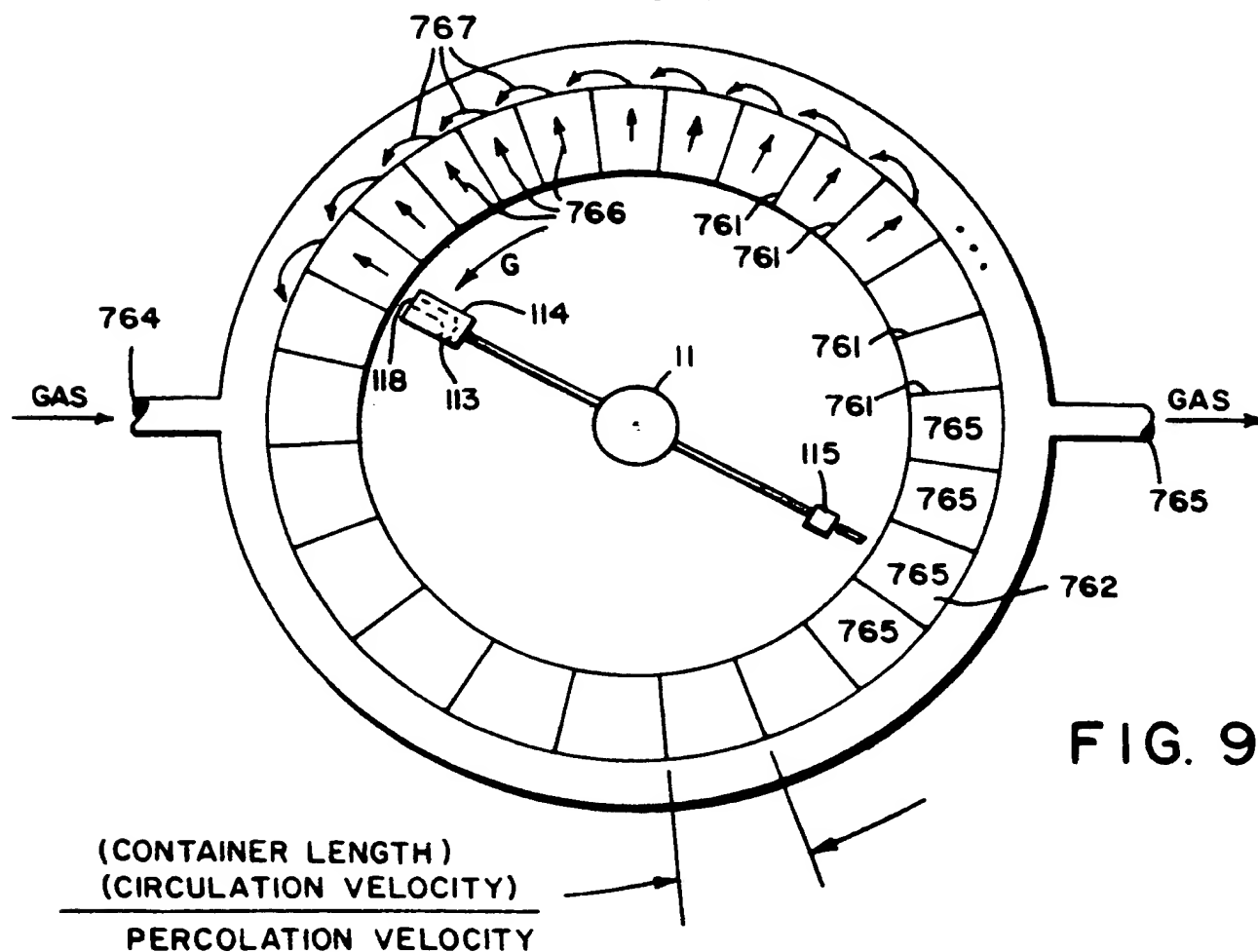


FIG. 9

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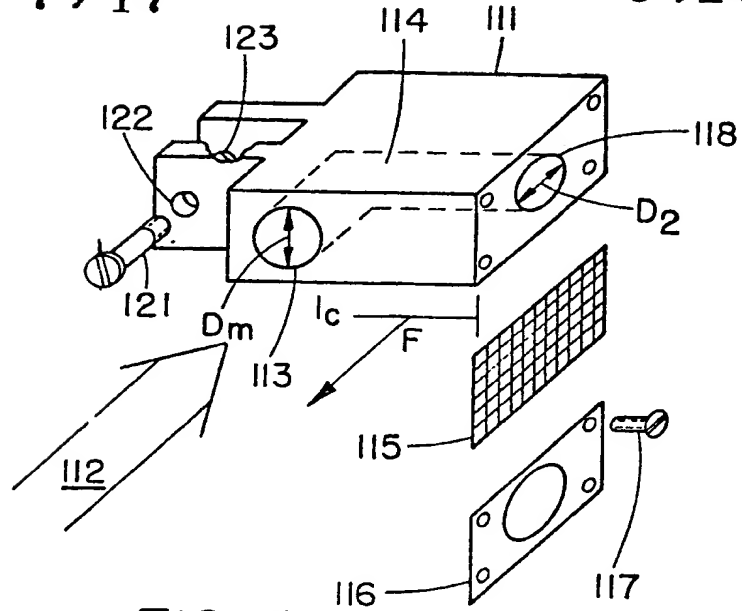


FIG. 10

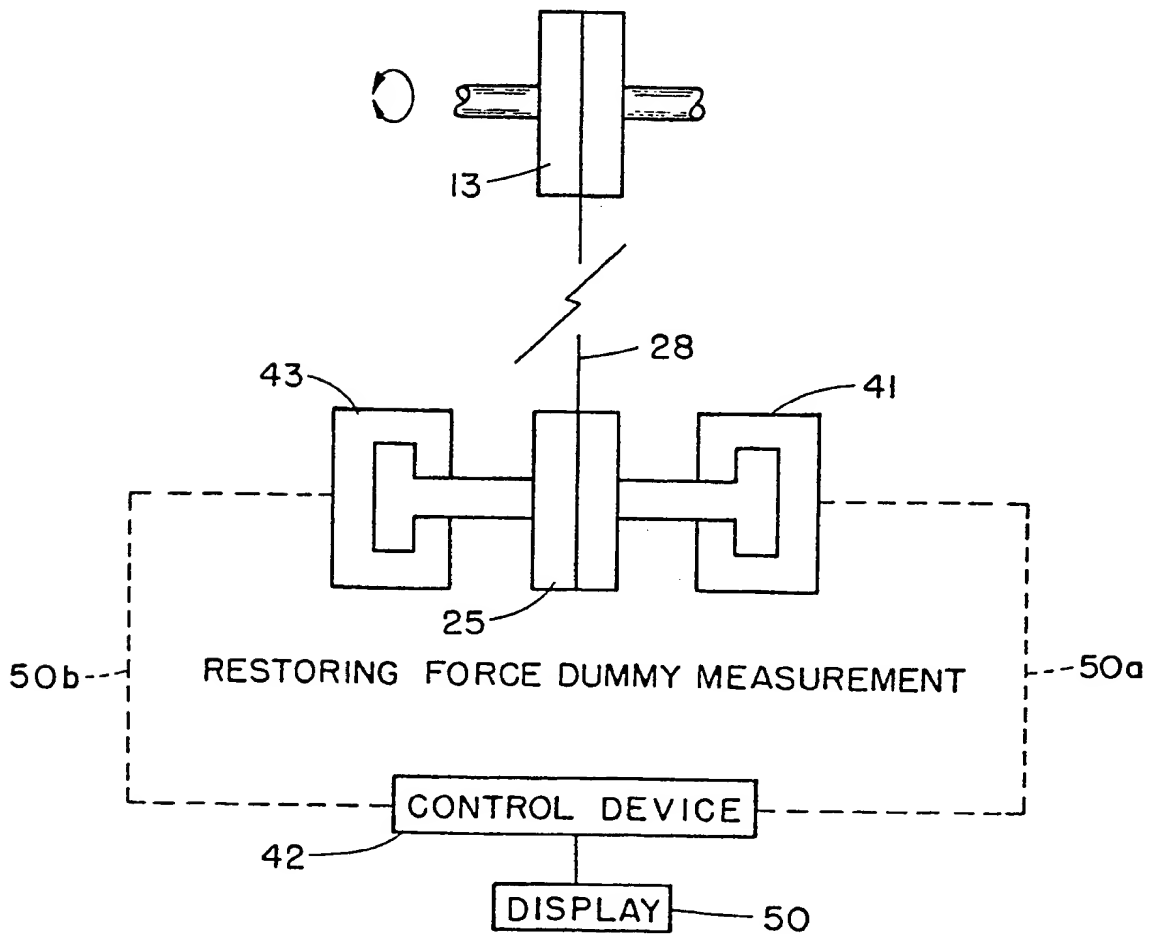
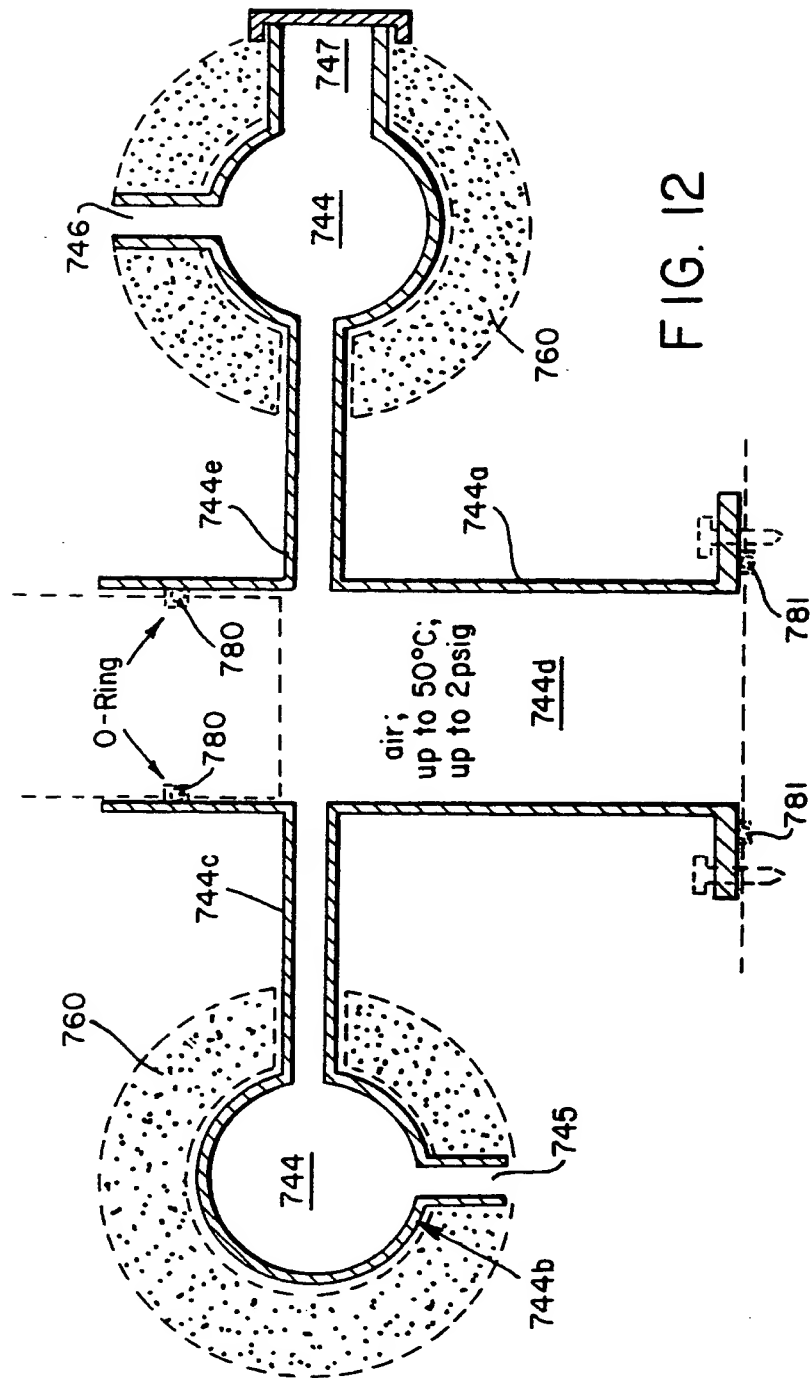


FIG. 11



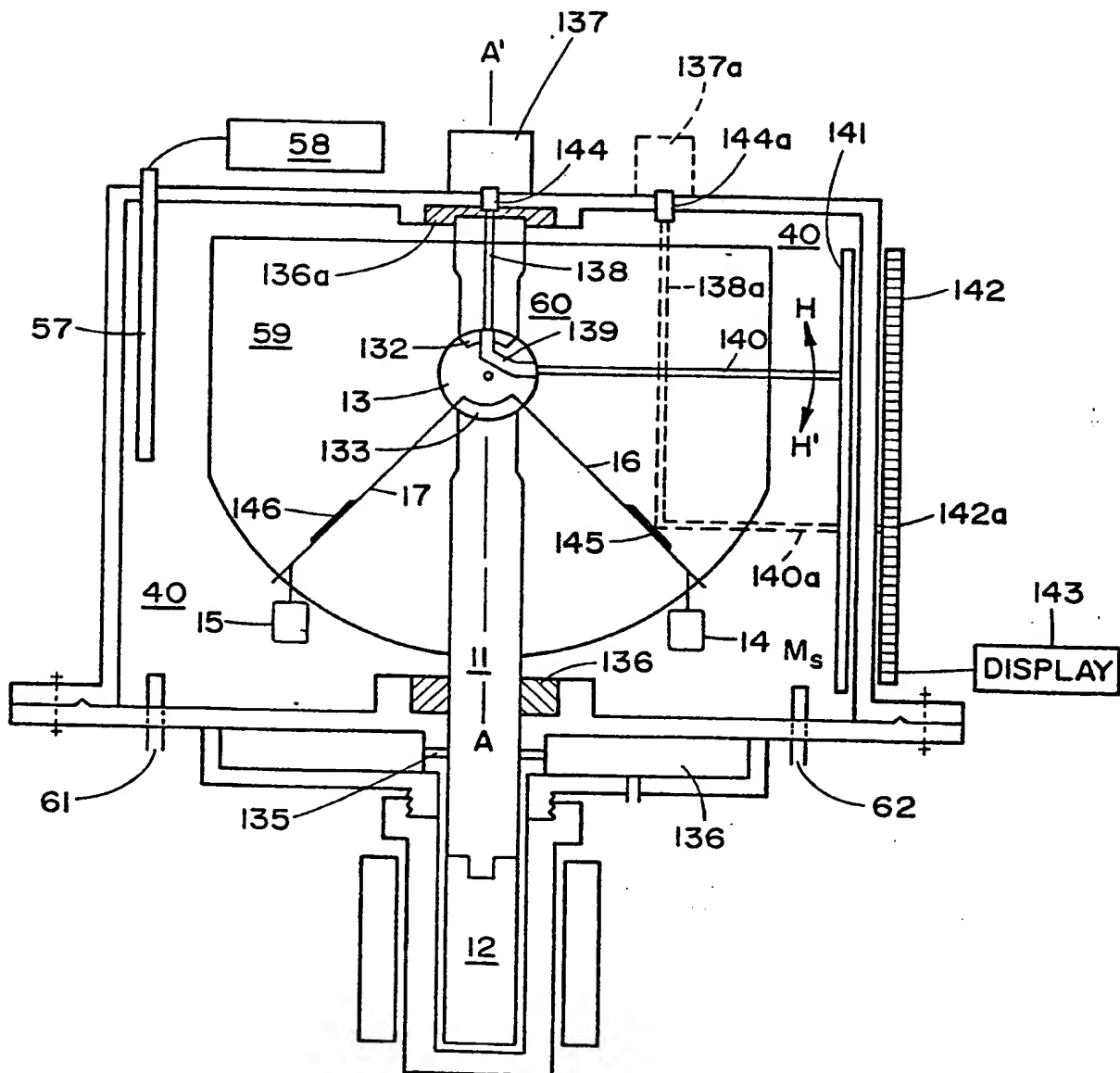


FIG. 13

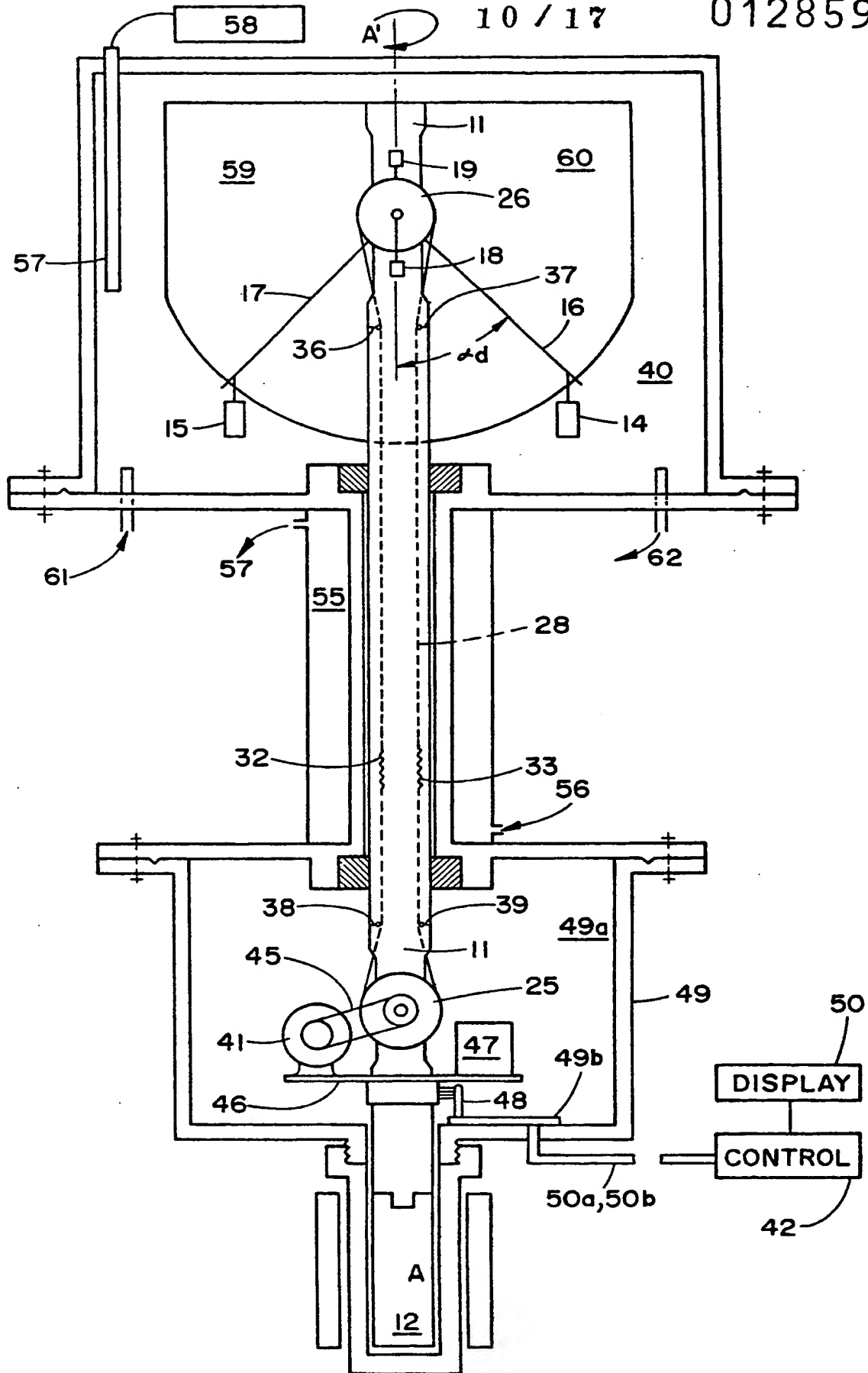


FIG. 14

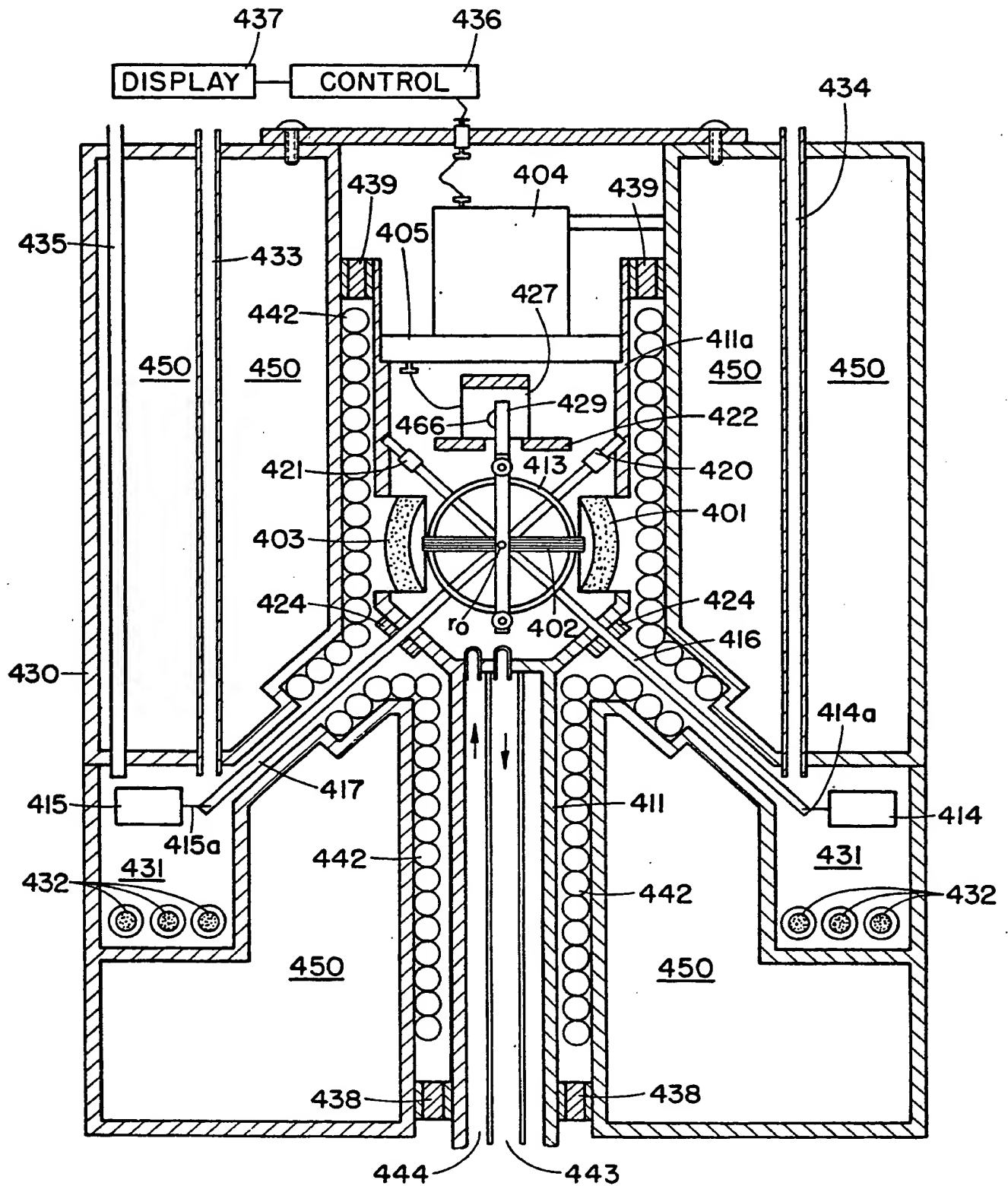


FIG.15

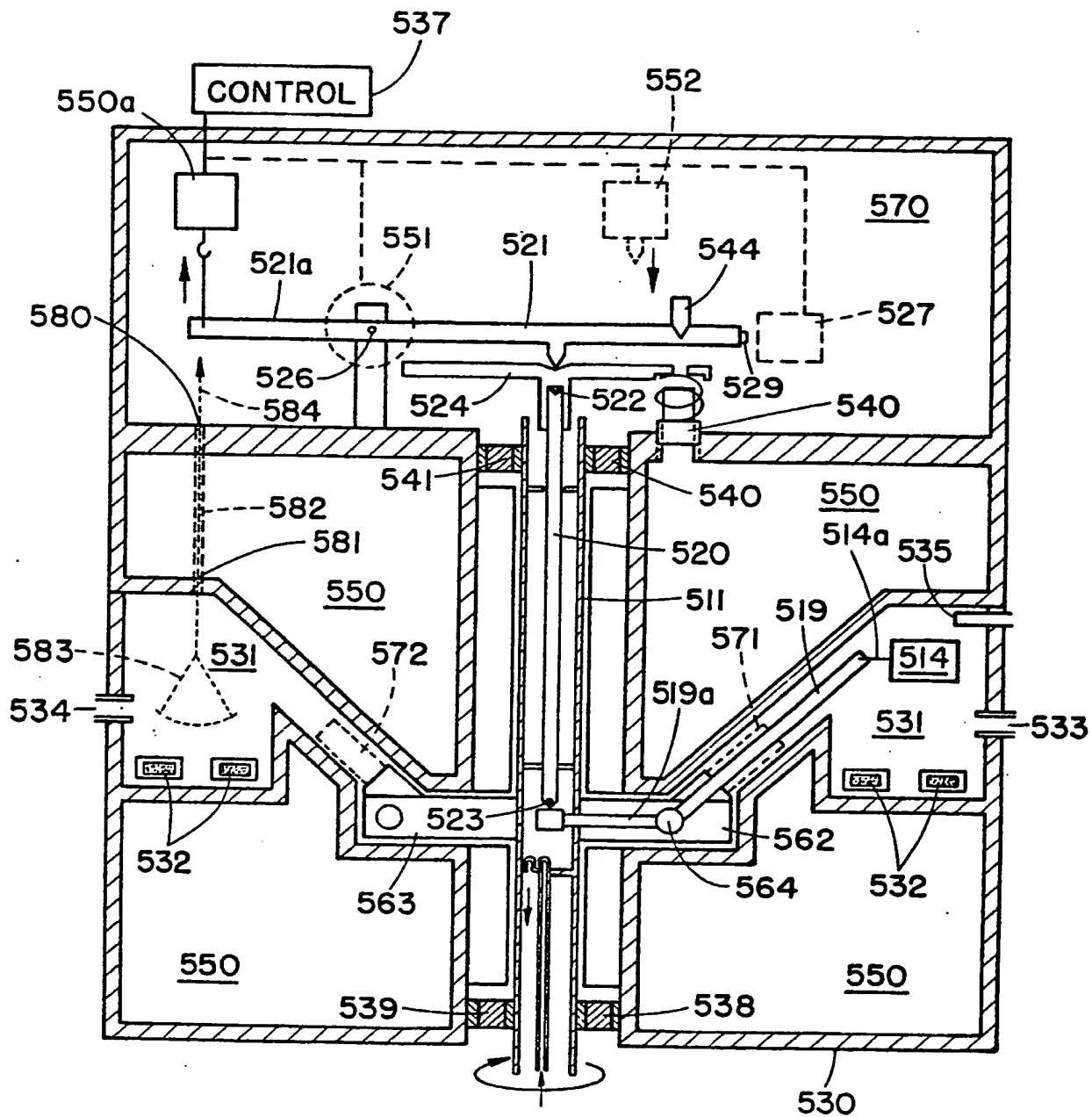


FIG. 16

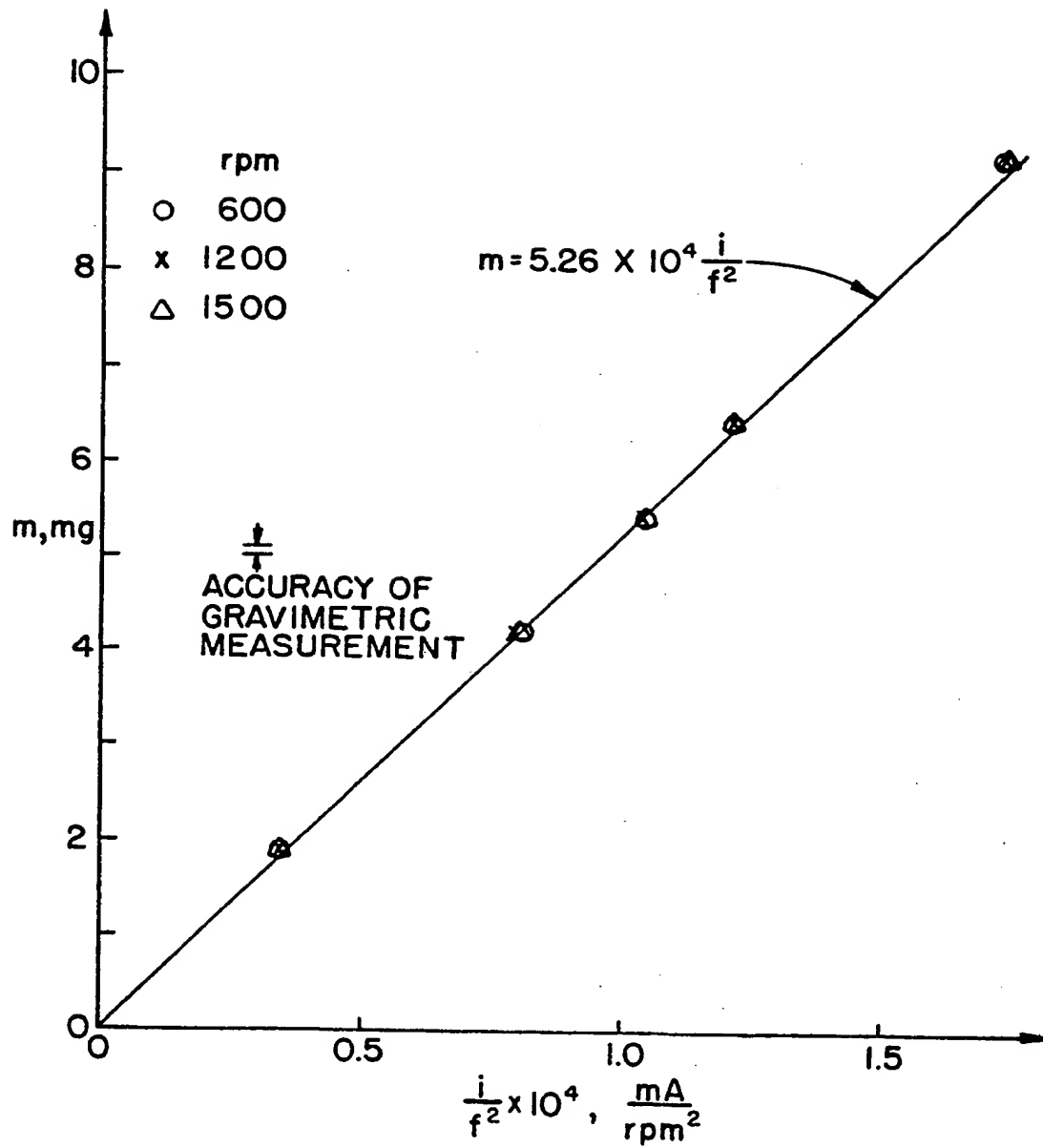


FIG.17

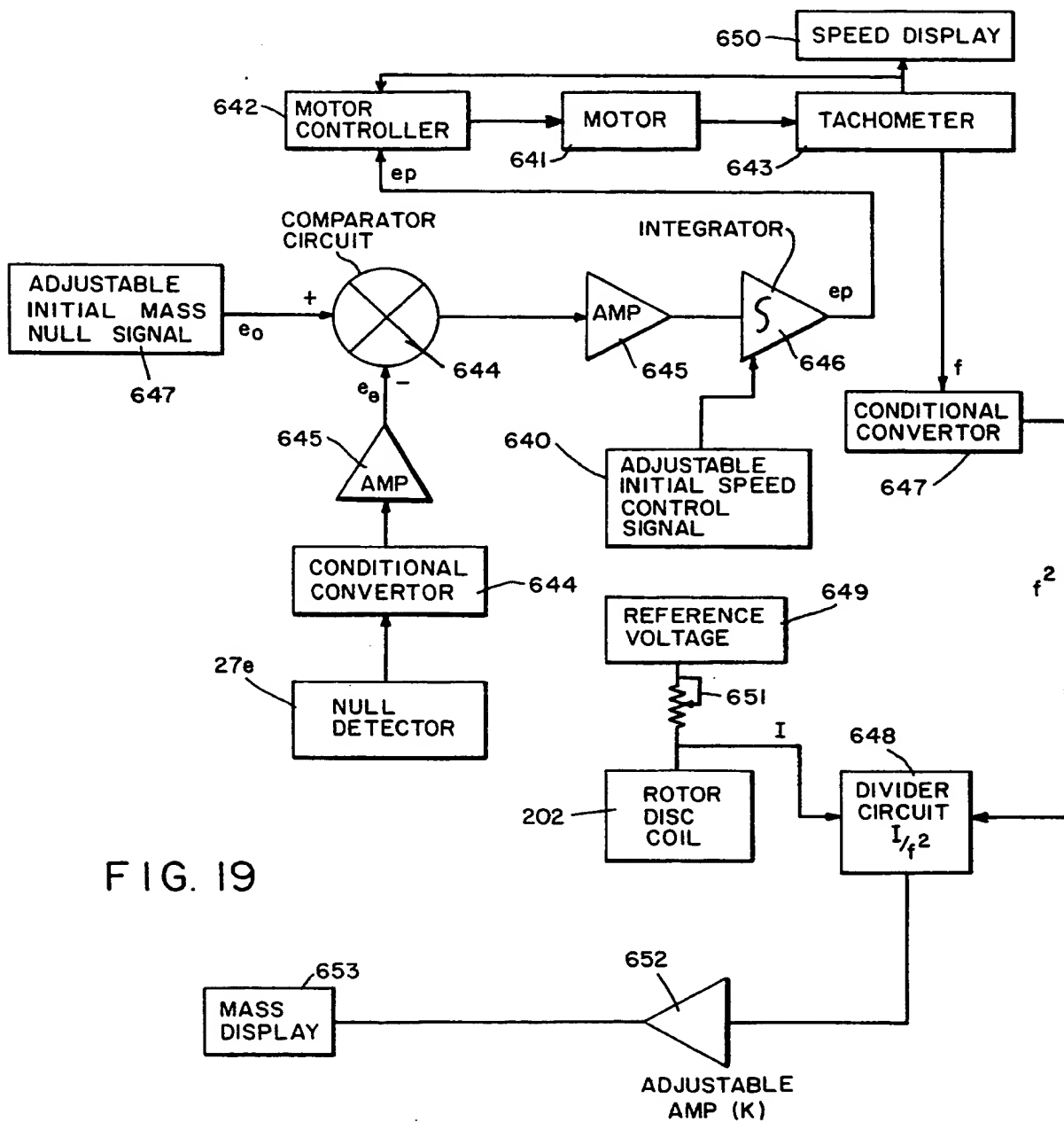
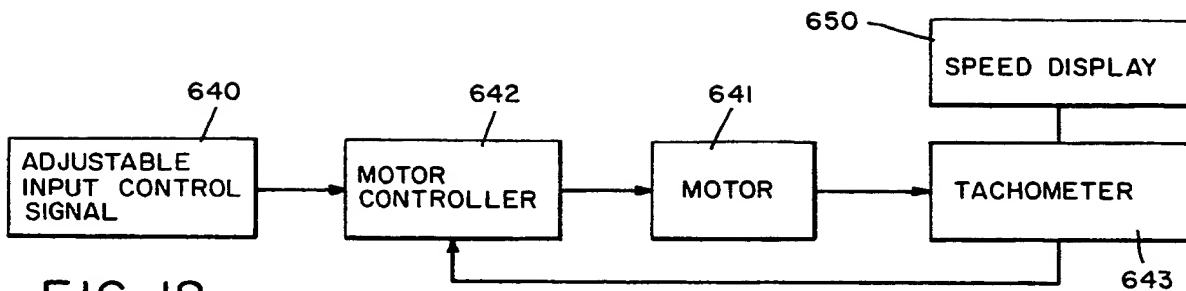


FIG. 20

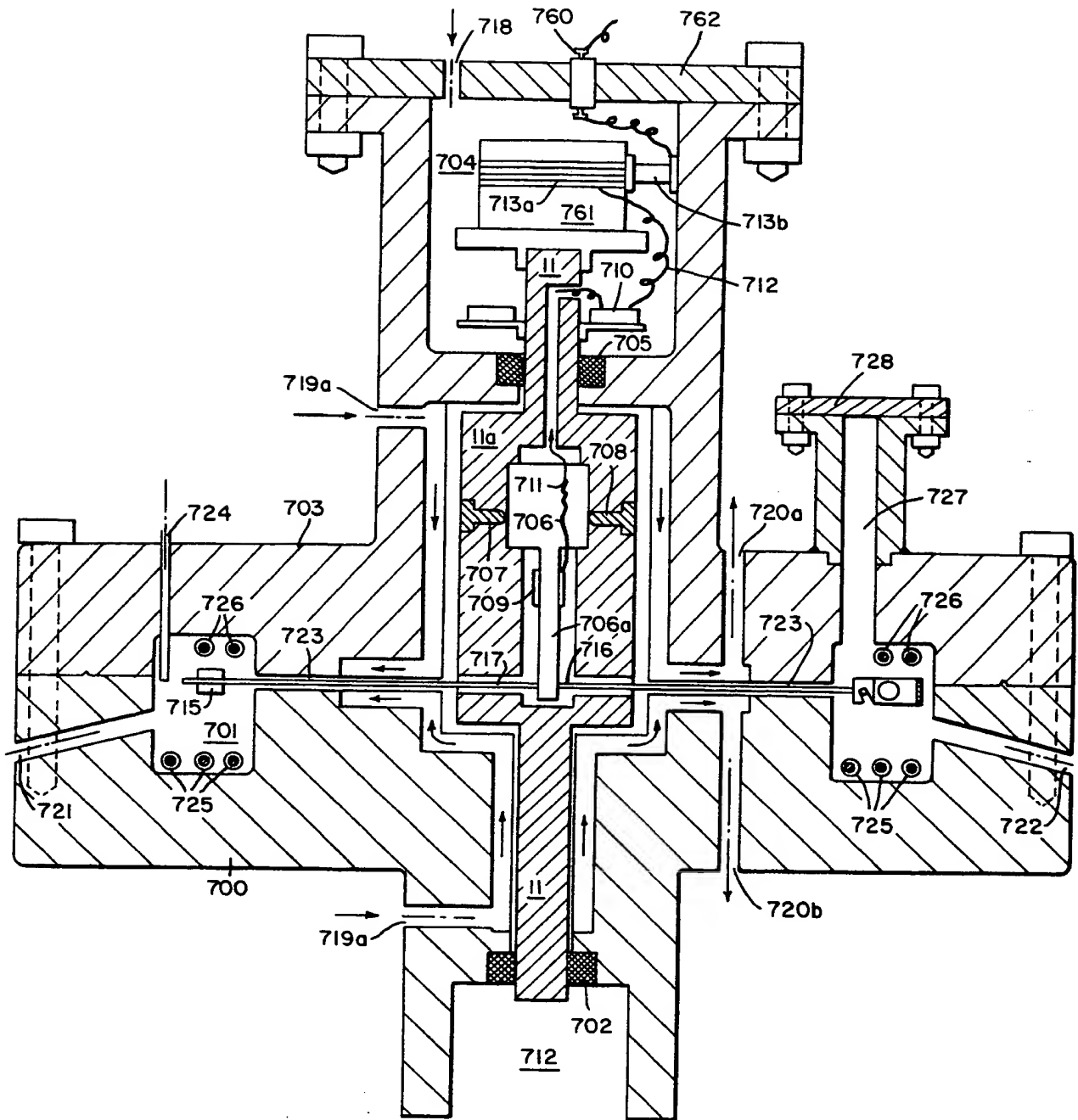


FIG. 21

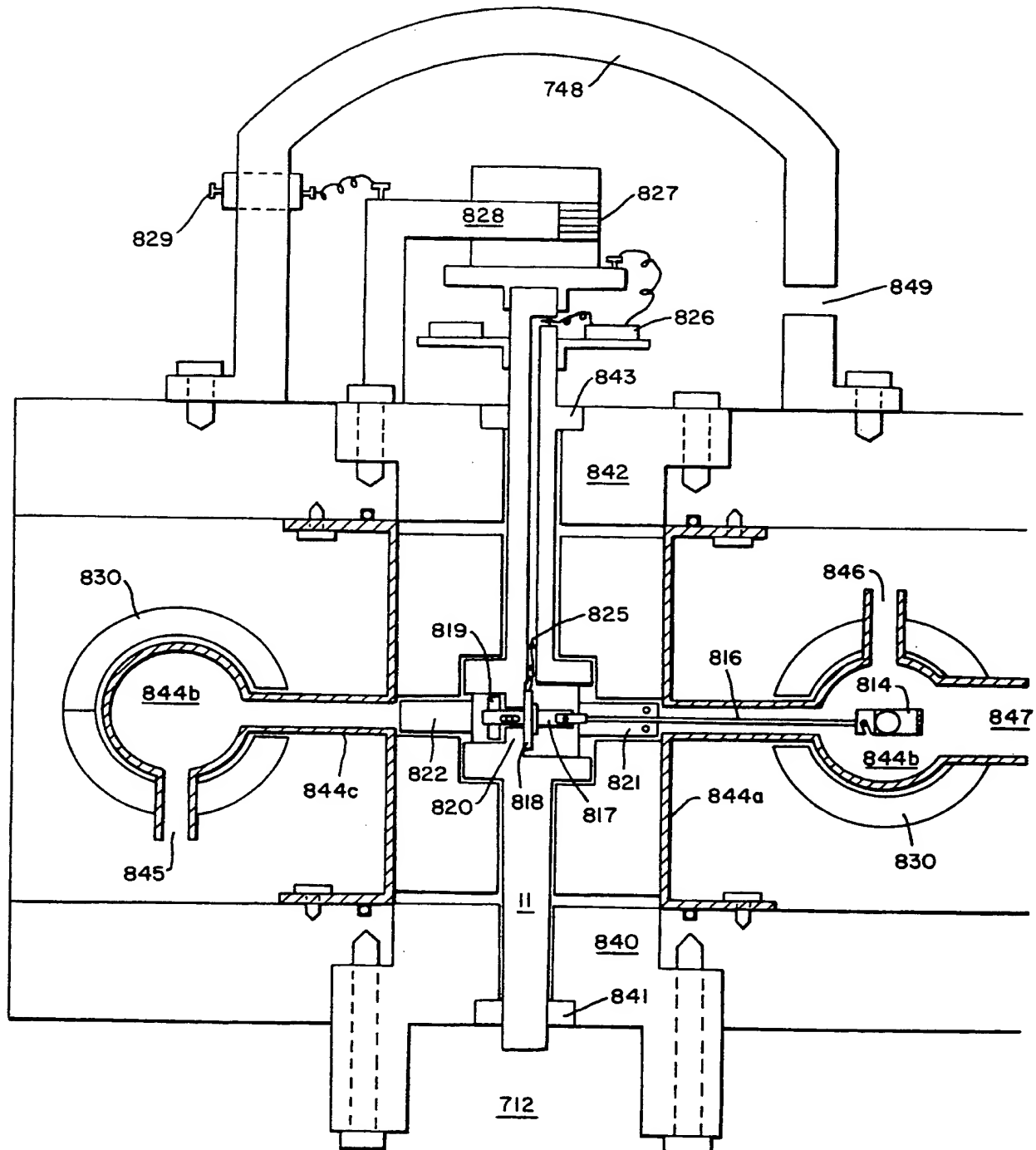
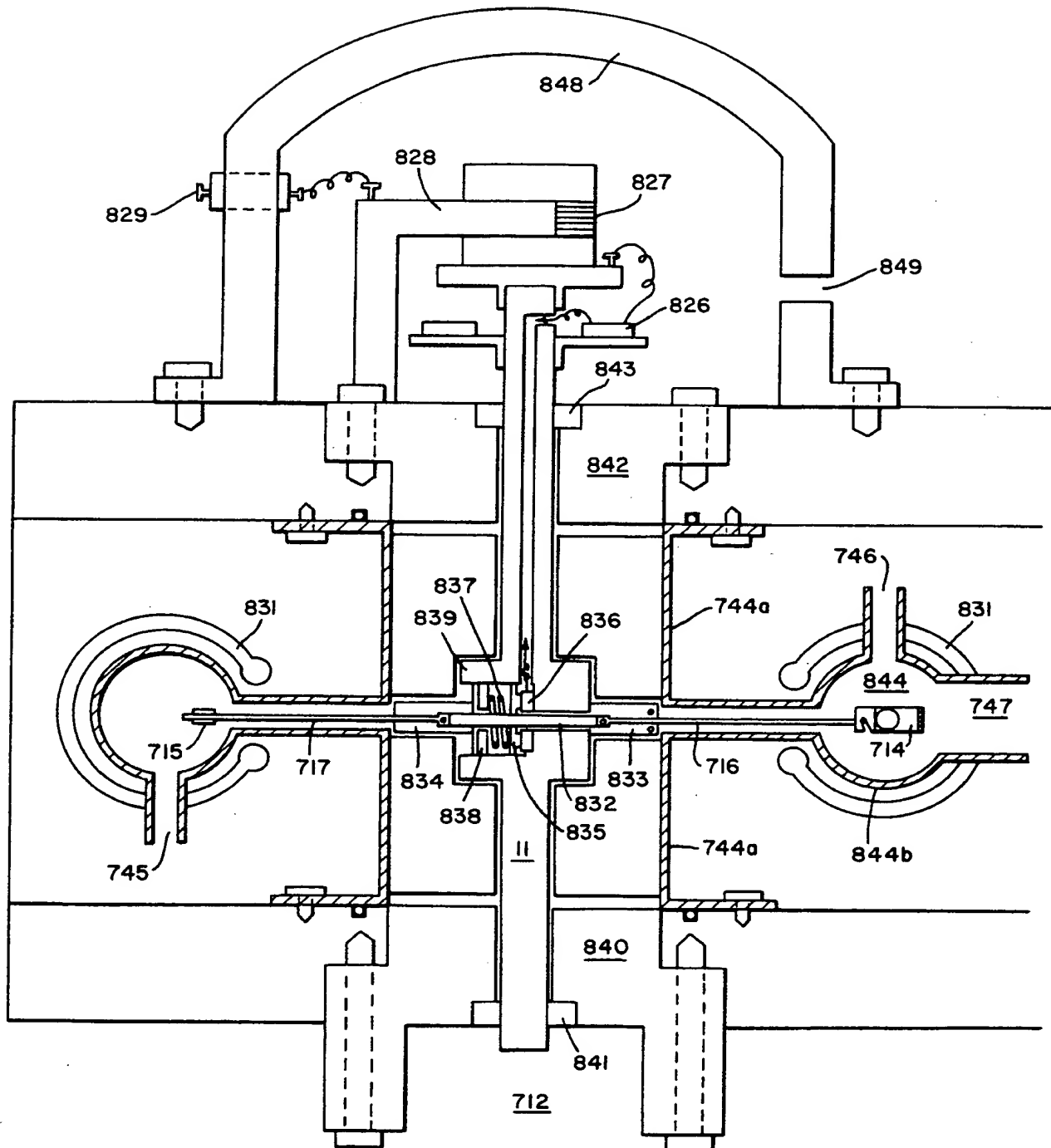


FIG. 22





European Patent
Office

EUROPEAN SEARCH REPORT

0128590

Application number

EP 84 10 6766

DOCUMENTS CONSIDERED TO BE RELEVANT			
Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	CLASSIFICATION OF THE APPLICATION (Int. Cl. 3)
D,A	US-A-3 973 636 (H. UCHIDA) * abstract; column 1, line 1 - column 2, line 41 *	1	G 01 N 5/00 G 01 N 9/30
D,A	--- US-A-3 812 924 (J.C. FLETCHER et al.) * column 1, lines 36-68 *	1	
A	--- US-A-3 981 178 (L.R. JONES et al.) -----		
			TECHNICAL FIELDS SEARCHED (Int. Cl. 3)
			G 01 N 5/00 G 01 N 9/00
The present search report has been drawn up for all claims			
Place of search THE HAGUE		Date of completion of the search 19-09-1984	Examiner ERRANI C.
CATEGORY OF CITED DOCUMENTS			
X : particularly relevant if taken alone Y : particularly relevant if combined with another document of the same category A : technical background O : non-written disclosure P : intermediate document		T : theory or principle underlying the invention E : earlier patent document, but published on, or after the filing date D : document cited in the application L : document cited for other reasons & : member of the same patent family, corresponding document	

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